## Preston Avenue and Baldwin Avenue Corridor Study



Meriden, CT
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## 1 Introduction

Fuss and O'Neill has prepared this Corridor Study for the South Central Regional Council of Governments (SCRCOG) on behalf of the City of Meriden to evaluate the existing transportation performance of Preston Avenue and Baldwin Avenue from East Main Street to Bee Street. Preston Avenue runs approximately 6,000 ' north/south between East Main Street and Interstate 91 while Baldwin Avenue is a continuation of Preston Avenue and is approximately $4,000^{\prime}$ long in an east/west orientation between Interstate 91 and Bee Street. A project location map is presented in Figure 1.

This study will be used as a planning tool by the City to evaluate and prioritize potential roadway improvements along the corridor. This study establishes the existing conditions of the roadway which will include pavement conditions, sight distances, drainage, utilities, and geometry. The study will identify existing deficiencies and will recommend potential improvements. Construction cost information is provided so that the City can prioritize improvements within the corridor.

## 2 Existing Conditions

A comprehensive field inventory of the study area roadway system was performed in April 2010. The inventory included documentation of existing roadway and intersection geometry, pavement conditions, sidewalk presence, drainage systems, and traffic control devices along the corridor.

### 2.1 Overview of Corridor

### 2.1.1 Preston Avenue

Preston Avenue is a two lane roadway oriented in a north-south direction, connecting Interstate 91 to East Main Street. Preston Avenue is bisected by Route 66 and is fronted by a number of land uses. The Connecticut Police Academy, Meriden Executive Office development, a handful of small businesses, and various residential properties are all located on Preston Avenue. The roadway is functionally classified as an Urban Minor Arterial according to the Connecticut Department of Transportation (CTDOT) and has a posted speed limit of 35 miles per hour. There is no on-street parking or bicycle facilities along this roadway and sidewalks are limited.

Automated traffic recorder counts were collected on Preston Avenue, south of the I-91 ramps, in June 2010. The counts were collected bi-directionally over a 48 -hour period along with speed data. Based on the counts, the existing weekday average daily traffic on Preston Avenue is 3,900 vehicles per day, with 1,700 vehicles traveling northbound and 2,200 vehicles traveling southbound. The $85^{\text {th }}$ percentile speed for Preston Avenue, south of the I-91 ramps was 44 miles per hour northbound and 47 miles per hour southbound. Based on field observations and roadway geometry, this should not be considered the uniform speed of traffic. Further speed evaluations should be performed along the corridor. Automated traffic recorder counts data are presented in Appendix A.

### 2.1.2 Baldwin Avenue

Baldwin Avenue is a two lane roadway oriented in an east-west direction, continuing from Preston Avenue at Interstate 91 to its termination at North Wall Street, west of Route 15. The corridor study limit, Bee Street, is located between Interstate 91 and Route 15. The land use on Baldwin Avenue is primarily residential with some commercial development near Interstate 91. The posted speed limit is 25 miles per hour. Baldwin Avenue is classified as an Urban Collector Street by CTDOT for most of its length. The segment between the Interstate 91 on and offramps is classified as an Urban Minor Arterial. There is no on-street parking or bicycle facilities along this roadway. Sidewalks are present along most of Baldwin Avenue, though discontinuities exist.

Automated traffic recorder counts were collected on Baldwin Avenue; however, the recorder was damaged during the data collection process and no data was retrievable.

### 2.2 Existing Roadway Segments and Intersection Conditions

There are seven distinct road segments (each about a quarter mile long) and are presented linearly in terms of geography, from East Main Street to Bee Street. Each roadway segment description includes a summary of the geometry, roadway widths, and pavement condition. The intersections that are present within each particular roadway segment are further described with the relevant intersection sight distance at stop-controlled intersections, pavement conditions, drainage structures present, and pavement marking condition. Town GIS data was utilized in reviewing existing horizontal and vertical geometry.

Intersection sight distances were measured at each intersection in accordance with criteria set forth in the 2003 CTDOT Highway Design Manual. Adequate intersection sight distances are required for intersection designs to maintain safe sight distances for motorists to enter or cross an intersection safely without disrupting the flow of traffic on the roadway. Intersection sight distances are a desired requirement while stopping sight distances are required.

Design criteria to be followed are listed in CTDOT's Highway Design Manual, 2003 edition. Specifically, relevant guidelines are shown for 3R Non-Freeway Projects classified as Minor Urban Arterials and Urban Collector Streets. The selected design speed was based on the CTDOT HDM for a Minor Urban Arterial and an Urban Collector Street in a suburban area. This speed is 5 miles per hour above the posted speed limit and is appropriate for the residential context of the corridor. This study analyzes the existing roadway through context sensitive design (CSD) procedures.

CSD, as defined by the Federal Highway Administration, is "a collaborative, interdisciplinary approach that involves all stakeholders to develop a transportation facility that fits its physical setting and preserves scenic, aesthetic, historic and environmental resources, while maintaining safety and mobility." One of design controls that CSD differs from historical practice is the use of speed data. Historically, it has been the practice to design the roadway for the $85^{\text {th }}$ percentile speed. This approach has the potential to promote speeds that are not consistent with the adjacent land use/environment. It should be noted that the CSD approach as used herein may
underestimate geometric related deficiencies. In these instances, increased enforcement and traffic calming measures should be considered.

According to the Manual, design parameters for Minor Urban Arterials, Figure 2-3H (Suburban Areas, 40 mph design speed) are:

- Travel lane width: $11^{\prime}-12^{\prime}$
- Shoulder width (non-NHS): 2' - 8'
- Parking lanes: $\mathrm{N} / \mathrm{A}$
- Bike lanes: $5^{\prime}$, if present
- Sidewalk width: $5^{\prime}$ minimum, if present
- Stopping sight distance: $305^{\prime}$
- Intersection sight distance: $445^{\prime}$
- Minimum Radius: 655' (Low Speed Urban)
- Grade: $0.5 \%-12 \%$
- Sag Vertical Curve K-Value: 64 (Headlight) - 35 (Comfort)
- Crest Vertical Curve K-Value: 44
- Vertical clearance for bridges: $14^{\prime}-3^{\prime \prime}$

According to the Manual, design parameters for Urban Collector Street, Figure 2-3H (Suburban Area, 30 mph design speed) are:

- Travel lane width: $10^{\prime}-12^{\prime}$
- Shoulder width (non-NHS): 2' - 8’
- Parking lanes: $7^{\prime}-10^{\prime}$, if present
- Bike lanes: $5^{\prime}$, if present
- Sidewalk width: 5' minimum, if present
- Stopping sight distance: $200^{\prime}$
- Intersection sight distance: 335'
- Minimum Radius: 295' (Low Speed Urban)
- Grade: $0.5 \%-13 \%$
- Sag Vertical Curve K-Value: 37 (Headlight) - 20 (Comfort)
- Crest Vertical Curve K-Value: 19

Detailed accident data was requested from the City of Meriden's Police Department for the last five years on record from 2005 to 2010. To date, only a general accident summary has been received. The only accidents reported by the City to have occurred within the corridor are at the intersection of Preston Avenue at East Main Street / Pomeroy Avenue / Cone Avenue. According to the City of Meriden Police Department, 48 accidents have occurred at the intersection with 9 involving injuries. CTDOT accident data was researched from 2006-2008 for the intersections of Preston Avenue at Route 66 and Baldwin Avenue at I-91. The results of the analysis revealed that 5 accidents have occurred at the intersection of Preston Avenue at the Route 66 off-ramp and 4 accidents at the Baldwin Avenue at I-91 off-ramp intersection.

Additional details beyond the summary total were not provided. It is presumed from the roadway geometry and visual evidence, that these accidents follow typical patterns associated with intersections and roadways of this type. These patterns include roadside fixed objects and turning movement counts. The overall totals indicate no significant accident pattern exists. In addition, no fatalities were recorded.

### 2.2.1 Preston Avenue - East Main Street to Parker Road

This segment of Preston Avenue is approximately 1,150 ' long and rises in elevation from East Main Street to Parker Road. The profile grade of the roadway ranges between $8.0 \%$ and $9.0 \%$ from the East Main Street intersection for 600'. The profile then reduces to a grade of $4.8 \%$ towards Parker Road. There is a vertical sag curve at the intersection of East Main Street which has a K -value of 20 . This sag vertical curve is substandard for both headlight and comfort criteria. The horizontal geometry of Preston Avenue through this segment has many curves as it bends towards the west. The minimum horizontal radius is $700^{\prime}$. There is one travel lane in each direction and the


Protruding drainage inlet on southbound Preston Avenue before intersection with East Main Street roadway is $28^{\prime} \pm$ wide, providing $12^{\prime}$ travel lanes with $2^{\prime} \pm$ shoulders.

The pavement is in fair to poor condition with longitudinal cracking, edge raveling, and several patches. Pavement markings are in fair to poor condition and are fading at various spots. Various objects are located within the clear zone of the roadway segment including drainage and landscape features. For example, a drop inlet with a protruding cement cover is located on the right side of the street (southbound) approximately 300' from the East Main Street intersection. A number of other drainage inlets have outdated designs and may not be as effective in collecting surface runoff as desired. No sidewalks are present, though a number of pedestrians were observed during the field visit walking on the shoulder at the southern end of the corridor. Land uses along this segment include residential, nursing home, small business, and agricultural properties.

### 2.2.1.1 East Main Street / Pomeroy Avenue / Cone Avenue Intersection

Preston Avenue terminates at the intersection of East Main Street / Pomeroy Avenue / Cone Avenue. The intersection is signalized and has five legs: East Main Street to the east and west, Preston Avenue to the north, Cone Avenue to the southeast, and Pomeroy Avenue to the southwest. All of the roadways have two travel lanes, one in each direction. East Main Street is classified as an Urban Principal Arterial and has an exclusive left turn lane in the eastbound direction; all other turning movements occur from shared lanes. At this location, the major street, East Main Street, has a posted speed limit of 30 miles per hour.

An existing vertical sag curve on Preston Avenue exists at the intersection with East Main Street. Preston Avenue has a 60 degree approach angle at East Main Street. Intersection sight distance from Preston Avenue to the east was measured at $240^{\prime}$ and over 450' to the west. Some landscape obstructions are present which is minimizing intersection sight distance to the east. The


East Main Street at Preston Avenue / Pomeroy and Cone Avenues looking east measured intersection sight distance looking east is insufficient compared to the recommended intersection sight distance of $390^{\prime}$ and the required $250^{\prime}$ for stopping sight distance for a 35 mile per hour design speed for East Main Street.

Cone Avenue is classified as a Local Street and the northbound Cone Avenue approach is aligned at a 60 degree angle to East Main Street. Intersection sight distance to the west was measured at 205' and over 450' to the east. Significant topographical challenges obstruct the view to the west, namely a steeply sloped lot containing a residence set back approximately $65^{\prime}$ from the street. The measured intersection sight distance looking west is insufficient compared to the recommended intersection sight distance of $390^{\prime}$ and the required $250^{\prime}$ for stopping sight distance for a 35 mile per hour design speed for East Main Street.

Pomeroy Avenue is classified as a Local Street and is the fifth leg of the intersection which meets East Main Street at a 45 degree angle. Though it is offset 50 ' to the west of the Preston Avenue approach, the current traffic signal phasing treats these approaches in coordination. Intersection sight distance looking west was measured at 150 ' and $450^{\prime}$ ' looking east along East Main Street. A thick tree line bordering the roadway is a primary reason for reduced driver visibility towards the west. The measured intersection sight distance looking west is insufficient compared to the recommended intersection sight distance of $390^{\prime}$ and the required $250^{\prime}$ for stopping sight distance for a 35 mile per hour design speed for East Main Street.

A single pedestrian crosswalk extends from the northwest corner of the intersection to a location across East Main Street between Cone and Pomeroy Avenues. No sidewalks or curb ramps are present at either end and there are no pedestrian signal heads. The southern end of

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the crosswalk has a very small landing area and is a questionable terminus location. Due to the alignment of intersection approaches and corresponding vehicular traffic signals, it is difficult to use these signals as a secondary visual aid for safe street crossing. Pavement markings are in good to fair shape with some sections showing wear.

Inspection of pavement conditions revealed wear on every approach. Longitudinal cracking was observed on East Main Street, and extensive pavement distress was present on the other three approaches. A number of utility patches were implemented on the Preston and Cone Avenue approaches. Due to the topography of minor street intersection approaches, evidence of roadway ponding was observed at the bottom of the two northbound approaches. Gutters and catch basins on Preston Avenue diverted most water runoff from this approach into a watercourse, though adjacent curbing and driveways exhibited erosion. An off-street catch basin located in a landscaped area of the property to the northeast of the intersection was mostly occluded by debris. A gravel driveway on the right side of the Preston Avenue (southbound direction) intersects the road at its low point; thus, no catch basin is present here and runoff continues overland across the driveway and into the watercourse.

At the request of the City of Meriden, an intersection capacity analysis was performed for the East Main Street/Pomeroy Avenue/Cone Avenue Intersection. The analysis was conducted using Synchro Professional Software, version 7.0.

In discussing intersection capacity analyses results, two terms are used to describe the operating condition of the road or intersection. These two terms are volume to capacity ratio $(\mathrm{v} / \mathrm{c})$ and level of service (LOS).

The v/c ratio is a ratio of the volume of traffic using an intersection to the total capacity of the intersection (the maximum number of vehicles that can utilize the intersection during an hour). The $\mathrm{v} / \mathrm{c}$ ratio can be used to describe the percentage of capacity utilized by a single intersection movement, a combination of movements, an entire intersection approach, or the intersection as a whole.

LOS is a measure of the delay experienced by stopped vehicles at an intersection. LOS is rated on a scale from A to F, with A describing a condition of very low delay (less than 10 seconds per vehicle), and F describing a condition where delays will exceed 50 seconds per vehicle for unsignalized intersections and 80 seconds per vehicle for signalized intersections. Delay is described as a measure of driver discomfort, frustration, fuel consumption, and lost travel time. Therefore, intersections with longer delay times are less acceptable to most drivers.

LOS is generally used to describe the operation (based on delay time) of both signalized and unsignalized intersections, while v/c ratio is applied to signalized intersections only. These definitions for $\mathrm{v} / \mathrm{c}$ ratio and LOS, as well as the methodology for conducting signalized and unsignalized intersection capacity analyses, are taken from the "2000 Highway Capacity Manual" published by the Transportation Research Board.

Turning movement counts were collected in June 2010 at the intersection during the morning peak period ( $7 \mathrm{AM}-9 \mathrm{AM}$ ) and the afternoon peak period (4 PM - 6 PM ). The peak hours of the intersection were observed to be 7:30-8:30 AM during the morning and 4:45-5:45 PM during the afternoon. Signal timings were observed in the field. Turning movement count data
are presented in Appendix $A$. The results of the intersection capacity analysis for the 2010 weekday morning and afternoon peak periods are presented in Table 1. Copies of the Synchro analysis worksheets can be found in Appendix B.

Table 1
2010 Weekday Level of Service Analysis - Preston Avenue at East Main Street

|  | Weekday Morning Peak Hour |  |  |  | Weekday Afternoon Peak Hour |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach and <br> Movement | Delay <br> (sec) | LOS | Percentile <br> Queue <br> (feet) | v/c <br> Ratio | Delay <br> (sec) | LOS | Percentile <br> Queue <br> (feet) | v/c <br> Ratio |
| East Main St. Eastbound - <br> Left | 20.4 | C | 63 | 0.52 | 52.0 | D | 215 | 0.96 |
| East Main St. Eastbound - <br> Through/Right | 18.5 | B | 133 | 0.49 | 24.0 | C | 332 | 0.81 |
| East Main St. Westbound - <br> Left/Through/Right | 26.9 | C | 168 | 0.68 | 29.8 | C | 198 | 0.74 |
| Pomeroy Ave. Northbound - <br> Left/Through/Right | 16.9 | B | 17 | 0.03 | 21.3 | C | 19 | 0.05 |
| Preston Ave. Southbound - <br> Left/Through/Right | 22.0 | C | 60 | 0.43 | 86.0 | F | 245 | 1.03 |
| Cone Ave. Northwestbound - <br> Left/Through/Right | 43.0 | D | 112 | 0.68 | 44.5 | D | 136 | 0.69 |
| Overall | 24.5 | C | N/A | 0.56 | 44.5 | D | N/A | 0.81 |

The results of the analysis show that the LOS for the overall intersection and individual movements operate at LOS D or better for both peak hours except for the Preston Avenue southbound weekday afternoon peak hour approach, which operates at LOS F. In addition the v/c ratio for Preston Avenue southbound is above 1.00 during the weekday afternoon peak hour.

### 2.2.1.2 Parker Road Intersection

Parker Road meets Preston Avenue to form a stopcontrolled T-intersection. Parker Road is classified as a Local Street, is stop-controlled and has a single shared lane for all outbound turning movements. The intersection sight distance from Parker Road looking to the south was measured at 235 ' and over 450' looking north. The intersection sight distance looking south is inhibited by a steep slope adjacent to the road. The measured intersection sight distance looking south is insufficient compared to the recommended intersection sight


Drainage channel and inlet at intersection of Parker Road and Preston Avenue

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distance of $445^{\prime}$ and the required $305^{\prime}$ for stopping sight distance.
The pavement is in good condition on Parker Road, though it has a few repaired cracks. The stop bar marking on Parker Road is faded. The southbound lane of Preston Avenue exhibits extensive fatigue cracking and the northbound lane has a protruding utility cap in the intersection. On the northeast corner of the intersection, a drainage channel has been constructed to feed roadway runoff into an inlet. The inlet is of atypical design and is partially obstructed by leaves and branches.

### 2.2.2 Preston Avenue - Parker Road to Route 66 Off-Ramp

Preston Avenue between Parker Road and the Route 66 off-ramp spans a distance of approximately $750^{\prime}$ in a north-south orientation. The vertical profile drops from a high point at Clearfield Drive towards the Route 66 off-ramp. The profile grade within this section is approximately $1.8 \%$. The horizontal geometry of Preston Avenue through this segment is fairly straight with a few horizontal curves that have radii over 1,000 ' which provides a small deflection angle. There is one travel lane in each direction and the roadway width varies between $25^{\prime}$ and 28 '. Variable width shoulders are present on both sides of the road.

Longitudinal cracking is present along the entire segment as is evidence of small repair patches along the roadway. Pavement markings are faded along the length of the roadway. Outdating guide rail treatment such as wire rope rail and cable guide rail are present on the westbound side of the roadway in the vicinity of the Route 66 off-ramp intersection


Inadequate barrier on southbound lane of Preston Avenue

Some erosion of shoulder landscaping is present along the fill side of the roadway due to surface runoff. No curbs or gutters are present on the cut side. A drop inlet with a makeshift wood palette cover is located 300' north of the intersection with Clearfield Drive at the edge of the northbound lane shoulder. The land use along this segment is primarily residential.

### 2.2.2.1 Clearfield Drive Intersection

The intersection of Preston Avenue and Clearfield Drive is a 3-way minor street stop controlled intersection located 250 ' north of Parker Road at the top of a vertical crest. Clearfield Drive is classified as a Local Street and is a two lane roadway providing a single lane approach towards Preston Avenue. The measured intersection sight distance to the north is 265 ' and to the south is 390 '. The intersection sight distance is prohibited by a vertical crest curve looking south and roadside vegetation looking north. The measured intersection sight distance looking south is insufficient compared to the recommended intersection sight distance of 445', but meets the
required $305^{\prime}$ for stopping sight distance. The measured intersection sight distance looking north is insufficient compared to the recommended intersection sight distance of 445' and the required 305 ' for stopping sight distance.

The pavement condition at the intersection is poor, particularly along the Preston Avenue approaches which have evidence of extensive fatigue cracking and pothole formation. The surface has been patched multiple times and is rough. The stop bar on Clearfield Drive and lane markings on Preston Avenue are faded.


Preston Avenue southbound approach to Clearfield Drive intersection shows extensive

### 2.2.2.2 Route 66 Off-Ramp Intersection

Route 66 connects to Interstate 691 and is classified as an Urban Principal Arterial Expressway. The off-ramp is for the eastbound travel lanes of Route 66. Sight distances were not measured from the Route 66 off-ramp as the highway is not under the jurisdiction of the City of Meriden.

Like the previous intersections mentioned, the pavement on each approach shows signs of wear, with longitudinal cracking present along Preston Avenue. The off-ramp is


Outdated cable guide railing on Route 66 off-ramp missing a stop bar and the roadside barriers differ on each side of the ramp with outdated cable guide rail located on the south side of the ramp.

### 2.2.3 Preston Avenue - Route 66 OffRamp to Patton Drive

The segment of Preston Avenue that extends from the Route 66 off-ramp to Patton Drive is 2,450 ' long in a north-south orientation. The vertical profile drops from the Route 66 offramp to a low point at Patton Drive. The profile grade within this section ranges between $1.2 \%$ and $4.2 \%$. The sag vertical curve at Patton Drive has a K-value of 24 , which does not meet the criteria for sag curves for either headlight or comfort. The horizontal geometry of Preston


Avenue through this segment meanders from east to west with a minimum radius of 1,000 '. The roadway width varies between $24^{\prime}$ and $30^{\prime}$ with one variable width travel lane and shoulder in each direction.

This segment is in similar condition to previously described segments of Preston Avenue and contains numerous cracks and evidence of fatigue. A scupper on the northbound side of Preston Avenue on the bridge over Route 66 was completely filled with silt. The segment is primarily wooded with land use primarily residential with the exception of the police academy on the east side of Preston Avenue at the Route 66 on-ramp. There are several signs for deer crossing present.

### 2.2.3.1 Route 66 On-Ramp Intersection / Police Academy Driveway

The State Police Training Facility is located just north of Route 66 on Preston Avenue. The driveway to the facility is aligned with the Route 66 on-ramp to facilitate rapid interstate highway access, with a single stop sign at the end of the driveway providing intersection control.

The measured intersection sight distance looking south from the driveway is $360^{\prime}$ and looking north is 280'. Both measured intersection sight distances are insufficient compared to the recommended intersection sight distance of $445^{\prime}$ and only the required

Southbound approach to intersection with
Police Academy driveway and Route 66
 $305^{\prime}$ for stopping sight distance is met looking south. Vegetation inhibits sight distance looking south and a steep slope along the roadway affects sight distance looking north.

Both transverse and longitudinal cracks are present on the Preston Avenue approaches and lane markings are worn. Drainage catch basins are present on both sides of the road.

### 2.2.3.2 Patton Drive Intersection

Patton Drive is the entrance to a relatively new subdivision and meets Preston Road at a Tintersection with minor street stop control. Patton Drive has 4" stone curbing and drainage inlets on either side of its leg of the intersection. A sidewalk with a curb ramp is located on the north side of Patton Drive. The bottom of the ramp is not fully flush with ground and there are no pedestrian facilities on


Drainage basin on northbound (cut) side of Preston Avenue north of Patton Drive

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Preston Avenue in the immediate vicinity of the intersection.
Measured intersection sight distance to the south is $280^{\prime}$, and to the north is $365^{\prime}$. Both measured intersection sight distances are insufficient compared to the recommended intersection sight distance of $445^{\prime}$ and only the required $305^{\prime}$ for stopping sight distance is met looking north. A steep vegetated slope inhibits intersection sight distance in both directions. The pavement on the Preston Avenue approaches demonstrates wear, with some longitudinal cracking and a transverse utility patch aligned with Patton Drive.

### 2.2.4 Preston Avenue - Patton Drive to Baldwin Avenue

The segment of Preston Avenue that extends from Preston Avenue to Baldwin Avenue is 1,650' long in a north-south orientation. The vertical profile is gently rolling through this segment. Starting from the low point at Patton Drive, there are two high points and one low point between Patton Drive and Baldwin Avenue. The profile grade varies from $0.5 \%$ to $1.9 \%$. All of the vertical curves meet design criteria except for the sag vertical curve between Patton Drive and Baldwin Avenue. The K -value of the sag vertical curve is 49 , which does
 not meet design criteria for headlight but does meet the criteria for comfort. The horizontal geometry of Preston Avenue through this segment is fairly straight until it meets Baldwin Avenue where the roadway curves to the west with a radius of 800 '. The roadway width varies between $24^{\prime}$ and $40^{\prime}$ with one variable width travel lane and shoulder in each direction. There are no curbs present on east side of the roadway, except in the vicinity of Baldwin Avenue.

Significant pavement failure is noted on this segment with fatigue cracking of several types being present. Roadside barrier types are


Roadway features of Preston Avenue between Patton Drive and Baldwin Avenue inconsistent and are no longer functional. This section of Preston Avenue is the only one with sidewalks, which are present for about 1,000 ' on the west side of the roadway. The sidewalk ends just before the Interstate 91 overpass, and there is a $1,200^{\prime}$ discontinuity before a sidewalk begins again further down Baldwin Avenue as noted in future sections of this study. Adjacent land uses are low density residential, agricultural, and office uses.

### 2.2.4.1 Baldwin Avenue Intersection

Preston Avenue intersects Baldwin Avenue at a three-way intersection just south of Interstate 91. The northbound and westbound approaches are named Preston Avenue and the southbound approach is named Baldwin Avenue. Thus, Baldwin Avenue is a continuation of the through movement along Preston Avenue. Through movement on the main corridor occurs along a curve with a radius of $800^{\prime}$ in the vicinity of the intersection.

The intersection sight distance measured from


Looking north from the beginning of Baldwin Avenue to the Interstate 91 overpass. the minor street looking south is more than 450' to the crest of the roadway and more than $400^{\prime}$ to the Interstate 91 overpass looking north. An on-ramp to the interstate is located approximately $200^{\prime}$ north of the intersection on the east side of the roadway, while a driveway for two large office buildings is located $100^{\prime}$ south on the west side of the roadway.

The pavement on all approaches is in fair condition and there is some longitudinal and transverse cracking, as well as edge failure at the seam of the office park driveway and Baldwin Avenue. A sidewalk exists along the entire street frontage of the commercial property on the west side of the intersection. Some curbing is present on both sides of the roadway. Twin drainage pipes have outlets directly across the street from the westbound Preston Avenue approach. A wooden post and rail barrier is used to block vehicular entry to the drainage channel which is about $10^{\prime}$ lower than the roadway. On the southeast corner of the intersection, a drainage inlet and headwall are present approximately 15 ' from the edge of the travel lane, and are surrounded by a handful of damaged wooden posts. There are no wires between the posts.

### 2.2.5 Baldwin Avenue - Preston Avenue to Preston Drive

Baldwin Avenue begins as a continuation of Preston Avenue just south of Interstate 91 and extends from Preston Avenue to Preston Drive. The segment is 1,200 ' long and is oriented in an east-west direction. The vertical profile descends from Preston Avenue ranging from $0.5 \%$ to $2.7 \%$. The horizontal geometry of Baldwin Avenue through this segment is primarily in a curve with a radius of $800^{\prime}$. This particular segment of Baldwin Avenue is wider than most of Preston Avenue. The roadway provides 13 ' $\pm$ travel lanes with variable width shoulders for


Baldwin Avenue at Interstate 91 overpass. a total width of approximately $40^{\prime}$. On the
north/westbound side of the roadway, the shoulder is a minimum of 2' wide, expanding to $5.5^{\prime}$ in some places. On the south/eastbound of the roadway, the paved shoulder varies in width from 4' to 8 '.

The pavement condition of this segment is fair, though in general, the Baldwin Avenue segments of the corridor are in better shape than the Preston Avenue ones. Fatigue cracking is more prevalent along Baldwin Avenue than on side streets, and there is minor edge wear. The vertical clearance of Baldwin Avenue under Interstate 91 is $13^{\prime}-10^{\prime \prime}$, which is below the design criteria of $14^{\prime}-3^{\prime \prime}$.

Curbs, gutters, and drainage basins are located along both sides of this segment, however they are intermittent. As Baldwin Avenue continues westward, the land use becomes primarily residential.

### 2.2.5.1 Thurrott Avenue Intersection

Thurrott Avenue intersects Baldwin Avenue just west of the Interstate 91 off-ramp; the minor road is stop-controlled. Thurrott Avenue is classified as a Local Street. The measured intersection sight distances to the west and east is $300^{\prime}$ and more than $350^{\prime}$ to the Interstate 91 Bridge, respectively. The measured intersection sight distance looking west is insufficient compared to the recommended intersection sight distance of 335'; however, it meets the required $200^{\prime}$ for stopping sight distance.

In the vicinity of the intersection, roadside


Looking east from Thurrott Drive along Baldwin Avenue barriers exist to prevent vehicles from entering drainage ditches on the north side of the road. The barrier between the off-ramp and Thurrott Avenue is not functioning properly as the cables are slack and posts are not all upright. Pavement condition is good, with some minor longitudinal cracks on the Baldwin Avenue approaches.

### 2.2.5.2 Preston Drive Intersection

Preston Drive intersects Baldwin Avenue 220 ' west of Thurrott Avenue to form a Tintersection. Preston Drive is classified as a Local Street and forms the stop-controlled minor leg of the three-way intersection. Looking east, the measured intersection sight distance $500^{\prime}+$ and looking west, the intersection sight distance is $300^{\prime}$. The measured intersection sight distance looking west is insufficient compared to the


Drainage and pavement condition on Baldwin Avenue east of Preston Drive

FUSS \& O'NEILL
recommended intersection sight distance of $335^{\prime}$; however, it meets the required $200^{\prime}$ for stopping sight distance.

Catch basins are located along the north side of the street on both Baldwin Avenue approaches and there is some curbing along the south side of the street with additional drainage inlets. Pavement condition is fair and some roadway patching has been performed on Baldwin Avenue in the vicinity of the intersection.

### 2.2.6 Baldwin Avenue - Preston Drive to Higby Drive

The segment of Baldwin Avenue between Preston Drive and Higby Drive is 1,350' long in an east-west orientation. The vertical profile is rolling through this segment. Starting from Preston Drive, the profile descends to a low point east of Heather Heights. The profile then ascends to a high point at Heather Heights before descending towards Higby Drive. The maximum profile grade is $11.6 \%$ between Lori Lane and the low point. All other grades vary between $1.0 \%$ and $5.2 \%$. The two vertical sag curves within this segment do not meet the Kvalue for headlight criteria but do meet the requirements for comfort criteria. The K-value for the vertical crest curve at Heather Heights does not meet the minimum value for 17 . The horizontal geometry of Preston Avenue through this segment is on a tangent from Preston Avenue to Lori Lane. The roadway then turns to the south with a $1,000^{\prime}$ radius curve and is in a tangent section until Heather Heights. The roadway turns towards the north to the east of Heather Heights with a 550 ' radius curve towards Higby Drive. The roadway width varies between $22^{\prime}$ and 36 ' with one variable width travel lane and shoulder in each direction.

There are several drainage basins located near Preston Drive, at Lori lane, and one approximately 350 ' east of the intersection with Heather Heights on the south side of Baldwin Avenue. An underground pipe conveys water from the basin 350 ' from Heather Heights to an outlet on the other side of the street. There are no roadside barriers preventing vehicular entry into the drainage ditch. In the eastbound direction, a sign depicting an upcoming junction with Interstate 691 is missing the highway shield. The damaged sign is located $400^{\prime}$ east of the Heather Heights intersection.


Top: Drainage basin, damaged highway sign, fatigued pavement, and incomplete sidewalk Bottom: Unprotected outlet across the street from the catch basin

In general, pavement along this roadway section shows signs of fatigue cracking and patching. The lane markings are faded as well as crosswalk
lines where present. Sidewalk coverage is mostly present on at least one side but switches back and forth across Baldwin Avenue. There are noticeable irregularities in pedestrian facilities (crosswalks, ramps, signing, etc.), which are important to rectify given the concentration of residential and recreational uses in the area.

### 2.2.6.1 Lori Lane Intersection

Lori Lane is classified as a Local Street and is a residential side street that meets Baldwin Avenue near a vertical crest to form a Tintersection, with Lori Lane stop controlled. The measured intersection sight distance is $400^{\prime}$ to the west and more than $600^{\prime}$ to the east.

The pavement is in good condition on all of the intersection approaches, with a few visible cracks on the major street, mainly on the westbound approach. Vegetation along the side slopes has crept into the shoulder


Looking east along Baldwin Avenue at Lori Lane space on the northern side of the road, so there is minimal pavement outside of the travel lanes at this location. There are no curbs on the northern (cut) side of the road, though some exist on the southern side along with a catch basin to the east of the intersection in a small swale. Though Lori Lane itself has sidewalks on both sides of the street, they do not extend to Baldwin Avenue and the intersection approaches do not have pedestrian facilities.

### 2.2.6.2 Heather Heights Intersection

Heather Heights and a new subdivision roadway are the side streets to form a 4-legged intersection located at the top of a vertical crest on Baldwin Avenue. Heather Heights is classified as a Local Street and is stop-controlled as well as the subdivision road. The measured intersection sight distances from both approaches looking east and west are greater than $335^{\circ}$.

The condition of the pavement is fair; the eastbound lane of Baldwin Avenue has fatigue cracking and multiple repair patches. The asphalt on the Heather Heights approach has been repaired with elastomeric crack filler. Curbs have been installed at the corners of the intersection but do not continue down Baldwin Avenue. One drainage inlet is present on Baldwin Avenue east of the intersection.

Sidewalks are present on every leg of the intersection, with the western and southern legs having sidewalks on both sides of the streets. Accordingly, three pedestrian ramps are present as well, located on every corner except the northeast corner. One faded crosswalk is painted across Heather Heights, though there is no crosswalk across Baldwin Avenue as the corresponding ramps are misaligned.

### 2.2.6.3 Higby Drive Intersection

Higby Drive is classified as a Local Street, is the minor leg of the T-intersection and is stop controlled. It is located directly across from green space and a walking trail entrance. The measured intersection sight distance looking to the west is $485^{\prime}$ and to the east is $375^{\prime}$.

The pavement condition of the approaches is fair. Baldwin Avenue has numerous cracks and small potholes in the vicinity of the intersection, some of which have been repaired. Curbing is present on the north side of the intersection and on the corners of the south side. Drainage inlets are not present and there is some erosion of landscaping on the southern side of the road where there are no curbs.

There are no sidewalks on Higby Drive, though there are pedestrian facilities adjacent to the westbound lanes of Baldwin Avenue in the intersection. The existing sidewalks have both impervious and pervious sections, and a gap of about 100 ' exists adjacent to the greenspace between the edge of the walking trail and Mattabassett Drive. A utility pole is located in the middle of the pedestrian travel


Sidewalk gap on westbound Baldwin Avenue approach to intersection with Higby Drive path in the gap.

### 2.2.7 Baldwin Avenue - Higby Drive to Bee Street

The segment of Baldwin Avenue extending from Higby Drive to Bee Street is 1,450 ' long in an east-west orientation. The vertical profile is rolling through this segment, starting from Higby Drive the profile descends to a low point west of Mattabassett Drive. The profile then ascends to a high point just east of Winding Brook Lane and descends to another low point just west of Winding Brook Lane. An additional high point is located 150 ' east of the Bee Street intersection. The profile grades range from $1.5 \%$ to $6.1 \%$. The crest and sag curve Kvalues between Mattabassett Drive and


Baldwin Avenue at Winding Brook Lane looking east Winding Brook Lane do not conform to the design criteria, however the sag curve K-value does conform to the comfort design criteria. The horizontal geometry of Baldwin Avenue is fairly straight with two horizontal curves with a minimum radius of $800^{\prime}$. The roadway width varies between $19^{\prime}$ and $26^{\prime}$ with one variable width travel lane and shoulder in each direction.

Unlike other segments of the corridor discussed earlier, this part of Baldwin Avenue has full sidewalk coverage along one side for its entire length. The pavement condition is good, with few cracks evident. Adjacent land use is primarily residential and recreational.

### 2.2.7.1 Mattabassett Drive Intersection

Mattabassett Drive intersects Baldwin Avenue to form a T-intersection with Mattabassett Drive stop controlled. Mattabassett Drive is classified as a Local Street. The measured intersection sight distance is approximately $550^{\prime}$ looking west and $270^{\prime}$ looking east. On the eastbound side of the street, a "limited sight distance" sign with flashing yellow lights is mounted to caution drivers about potential unseen roadway hazards on the other side of a vertical crest curve. The measured intersection sight distance looking east is insufficient compared to the recommended intersection sight distance of $335^{\prime}$, however meets the required $200^{\prime}$ for stopping sight distance.

A sidewalk is present on the north side of Baldwin Avenue. The sidewalk is elevated and separated from the roadway by a curb. There


Limited sight distance to west of intersection with Mattabassett Drive are no drainage basins or gutters on the south side of the road and there is evidence of minor erosion along the edge of the roadway. The pavement condition is fair in this area and does exhibit some longitudinal cracking and edge of road failure.

### 2.2.7.2 Winding Brook Lane Intersection

Winding Brook Lane intersects Baldwin Avenue west of a vertical crest curve to form a Tintersection, with Winding Brook Lane stop controlled. Winding Brook Lane is classified as a Local Street. The measured sight distance from this intersection is $195^{\prime}$ looking east and 290' being looking west. The measured intersection sight distance for both directions is insufficient compared to the recommended intersection sight distance of 335 ' and only the western sight distance meets the required $200^{\prime}$ for stopping sight distance.


Limited intersection sight distance looking east from Winding Brook Drive

The pavement has fatigue cracks on the Baldwin Avenue approaches as well as repaired transverse cracks on Winding Brook Lane. Similar to the Mattabassett Drive intersection, a sidewalk is present along the north side of the road. There is no curbing on the south side of the road and drainage inlets are not present in the vicinity of the intersection.

### 2.2.7.3 Bee Street Intersection

Bee Street crosses Baldwin Avenue at a 4 -way intersection with stop control on every approach. Intersection sight distances were measured from Baldwin Avenue for both approaches to Bee Street. The measured intersection sight distance on Baldwin Avenue westbound looking north is $500^{\prime}+$ and looking south is $295^{\prime}$. The measured intersection sight distance on Baldwin Avenue eastbound looking north is $500^{\prime}+$ and looking south is $475^{\prime}$. The measured intersection sight distance for the Baldwin Avenue westbound approach looking south is insufficient compared to the recommended intersection sight distance of $335^{\prime}$; however, it meets the required $200^{\prime}$ for stopping sight distance.

Sidewalks are present on several approaches, which connect area residences with recreational opportunities, including Carroll Park on the northwest corner of the intersection. Specifically, sidewalks are located alongside the following travel lanes: westbound Baldwin Avenue and northbound Bee Street. Two highly visible zebra


Sight obstruction on westbound approach to Bee Street / Baldwin Avenue intersection striped crosswalks connect these sidewalks and ramps are present at each end of the crosswalks.

The pavement condition on every approach is good, and there is little evidence of drainage problems at the intersection. Curb and gutters are installed on most legs and a creek and drainage area is fenced off adjacent to the park.

## 3 Drainage Analysis

A conceptual drainage analysis was performed to determine deficiencies and potential drainage improvements for the corridor. The existing drainage areas for the corridor were defined based on the City GIS data and the design flows were analyzed for the 25 -year storm. Proposed catch basin spacing was based on maximum recommended spacing. Detailed gutter analysis was not in the scope of this effort.

The Preston Avenue corridor has three existing low points between East Main Street and Baldwin Avenue. These low points are located at East Main Street, Patton Drive, and west of Baldwin Avenue.

A closed drainage system exists north of Parker Road to East Main Street and outlets at a watercourse at the northwest corners of East Main Street. The existing drainage area was delineated to be 8.8 acres. Based on the results of the conceptual drainage analysis, an 18 " outlet pipe would be required to handle the volume of water within this segment of roadway. The existing catch basin spacing does not meet the CTDOT recommended maximum spacing of 300 '.

A closed drainage system exists between Parker Road and the Route 66 off-ramp. The existing drainage area was delineated to be 1.7 acres. The existing outlet could not be field located. Based on the results of the conceptual drainage analysis, a 12 " outlet pipe should accommodate storm drainage through this segment. The existing catch basin spacing does not meet the CTDOT recommended maximum spacing of $300^{\prime}$.

A closed drainage system exists on the east side of Preston Avenue from the Route 66 on-ramp to north of Patton Drive. The existing drainage area was delineated to be 15.9 acres. The existing outlet could not be field located. Based on the results of the conceptual drainage analysis, a 24 " outlet pipe should accommodate storm drainage through this segment. The existing catch basin spacing does not meet the CTDOT recommended maximum spacing of $300^{\prime}$ on the east side of Preston Avenue. No catch basins exist on the west side as the existing ground slopes away from the roadway; however, debris and vegetation along the roadway act like a curb line directing storm water to the low point. In addition, flanker catch basins do not exist at the low point.

A closed drainage system exists between the north of Patton Drive and Baldwin Avenue. The existing drainage area was delineated to be 3.0 acres. The existing outlet to the system drains into the office park property. The existing outlet was not field measured; however, based on the results of the conceptual drainage analysis, an $18^{\prime \prime}$ pipe is necessary.

The Baldwin Avenue corridor has three existing low points between Preston Avenue and Bee Street. These low points are located at west of Heather Heights, at Mattabasset Drive, and between Winding Brook Lane and Bee Street.

A closed drainage system exists between Baldwin Avenue and Heather Heights. The existing drainage area was delineated to be 3.4 acres. The existing outlet to the system drains to the north of the roadway. The existing outlet was not field measured; however, based on the
results of the conceptual drainage analysis, an 18 " pipe is necessary. The existing catch basin spacing does not meet the CTDOT recommended maximum spacing of $300^{\prime}$ at various sections. In addition, flanker catch basins do not exist at the low point.

A closed drainage system exists between Heather Heights and Winding Brook Lane. The existing drainage area was delineated to be 1.7 acres. Based on the existing conditions survey from the "Baldwin Avenue Improvements" project, this drainage system connects to an existing 36" trunk line on Baldwin Avenue. It is assumed that the trunk line is adequately sized. The existing catch basin spacing does not meet the CTDOT recommended maximum spacing of $300^{\prime}$ at various sections. In addition, flanker catch basins do not exist at the low point.

A closed drainage system exists between Winding Brook Lane and Bee Street. The existing drainage area was delineated to be 0.7 acres. Based on the existing condition survey from the "Baldwin Avenue Improvements" project, this drainage system connects to the before mentioned 36 " trunk line. Flanker catch basins do not exist at the low point.

## 4 Future Developments

The City of Meriden has identified one future development that will have potential traffic impacts to the Preston Avenue/Baldwin Avenue corridor, the Hall Property planned development area. The Hall Property is approximately 70 acres of land and is located on the parcel formed by I-91, I-691/Route 66 and Preston Avenue. The property is currently zoned "S-R Suburban Residential" and was identified as a potential site to create sustainable, highquality commercial, office, and industrial space that would be designed in a manner that maximizes tax revenue while being sensitive to surrounding neighborhoods and environmental assets. One of the recommendations in the City's POCD is to change the zone for this property so that it can be developed for commercial use. The City has begun this effort and is in the process of developing the zone regulations for the zone change. Additionally, the City has also developed an initial concept for the site which includes:

- Townhouse: 300 units
- Retail: 200,000 square feet (sq. ft.)
- Office: 75,000 sq. ft.
- Hotel: 75,000 sq. ft.
- Fitness/Health Center: 50,000 sq. ft.
- Parking: 2,000 spaces

Estimates of the amount of traffic expected to be generated by this initial concept was made using Trip Generation, Version 6 which implements procedures in the Institute of Transportation Engineers (ITE) publication titled, Trip Generation, 7th edition. A summary of the site generated trips estimated is provided in Table 2.

Table 2
Hall Property Mixed-Use Development Initial Concept Site Generated Trips

|  | Land Use Code | Units | Daily | AM Peak Hour |  |  | PM Peak Hour |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  |  | Enter | Exit | Total | Enter | Exit | Total |
| Townhouse | 230 | 300 | 1,743 | 21 | 111 | 132 | 105 | 51 | 156 |
| Retail | 820 | $\begin{gathered} 200,000 \\ \text { sq. ft. } \end{gathered}$ | 8,588 | 122 | 78 | 200 | 366 | 380 | 746 |
| Office | 710 | $\begin{aligned} & 75,000 \\ & \text { sq. ft. } \\ & \hline \end{aligned}$ | 826 | 102 | 14 | 116 | 19 | 93 | 112 |
| Hotel | 310 | $\begin{aligned} & 75,000 \\ & \text { sq. ft.* } \\ & \hline \end{aligned}$ | 1,226 | 51 | 33 | 84 | 47 | 42 | 89 |
| Health/Fitness | 492 | $\begin{gathered} 50,000 \\ \text { sq. ft. } \end{gathered}$ | 1,647 | 31 | 38 | 69 | 100 | 76 | 176 |
| Total |  |  | 14,030 | 327 | 274 | 601 | 637 | 642 | 1,279 |
| Internal Capture Trips** |  |  | 1,122 | 26 | 22 | 48 | 51 | 51 | 102 |
| Total Site Trips |  |  | 12,908 | 301 | 252 | 553 | 586 | 591 | 1,117 |

Source: Fitzgerald \& Halliday, Inc., June 2010

* Assumes 1.95 rooms per 1,000 square feet.
${ }^{* *}$ Assumes an $8 \%$ internal capture rate.
Assuming an internal capture rate of $8 \%$, it is estimated that approximately 13,000 trips per day, 550 vehicle trips during the morning peak hour, and 1,200 vehicle trips during the afternoon peak hour will be generated by the proposed development.


## 5 Recommended Improvements

The existing conditions assessment served to identify existing roadway deficiencies along the Preston and Baldwin Avenue corridors. The purpose of this section of the report is to summarize potential improvements based on the identified existing deficiencies. Preliminary construction cost estimates were prepared for each roadway segment per CTDOT preliminary estimating procedures for the City to prioritize the implementation of the recommended improvements.

The projected Year 2030 weekday average daily traffic volumes for Preston Avenue, given a $1 \%$ annual growth rate and vehicle trips anticipated to be generated by the Hall Property, are estimated to be 17,750 vehicles per day with 8,600 vehicles traveling northbound and 9,150 vehicles traveling southbound. Based on these volumes, the two-lane Preston Avenue will not accommodate the projected Year 2030 weekday average daily traffic with the full build-out of the Hall Property. Mitigation measures for the full build-out of the Hall Property may include widening Preston and Baldwin Avenues from two lanes to four lanes between Route 66 and I91 with potential intersection capacity improvements at the proposed entrance to the site. A detailed traffic study will be required for the Hall Property to indentify specific improvements. Traffic counts were performed at the Preston Avenue at East Main Street / Pomeroy Avenue / Cone Avenue only and the results of the intersection capacity analysis are presented in the relevant section.

### 5.1 Preston Avenue - East Main Street to Parker Road

An intersection capacity analysis was performed for the East Main Street/Pomeroy Avenue/Cone Avenue intersection for the future Year 2030 traffic volumes. The projected Year 2030 weekday traffic volumes for the intersection were grown by a $1 \%$ annual growth rate. Additional traffic to be generated by the Hall Property development at the intersection was not estimated. A detailed trip distribution will be required when a traffic study for the Hall Property development is initiated. It is assumed that the traffic to be generated by the development at the intersection will be minor when compared to the future traffic volumes at the intersection.

The results of the intersection capacity analysis for the 2030 weekday morning and afternoon peak periods are presented in Table 3. Copies of the Synchro analysis worksheets can be found in Appendix C.

Table 3
2030 Weekday Level of Service Analysis - Preston Avenue at East Main Street

|  | Weekday Morning Peak Hour |  |  | Weekday Afternoon Peak Hour |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach and <br> Movement | Delay <br> (sec) | LOS | Percentile <br> Queue <br> (feet) | v/c <br> Ratio | Delay <br> (sec) | LOS | Percentile <br> Queue <br> (feet) | v/c <br> Ratio |
| East Main St. Eastbound - <br> Left | 27.8 | C | 76 | 0.70 | 174.1 | F | 317 | 1.31 |
| East Main St. Eastbound - <br> Through/Right | 19.8 | B | 162 | 0.58 | 48.9 | D | 447 | 0.98 |
| East Main St. Westbound - <br> Left/Through/Right | 38.6 | D | 244 | 0.85 | 53.3 | D | 271 | 0.94 |
| Pomeroy Ave. Northbound - <br> Left/Through/Right | 17.5 | B | 21 | 0.05 | 21.5 | C | 23 | 0.07 |
| Preston Ave. Southbound - <br> Left/Through/Right | 28.3 | C | 105 | 0.65 | 181.0 | F | 318 | 1.29 |
| Cone Ave. Northwestbound - <br> Left/Through/Right | 59.2 | E | 144 | 0.84 | 59.3 | E | 173 | 0.84 |
| Overall | 32.0 | C | N/A | $\mathbf{0 . 7 5}$ | $\mathbf{1 0 2 . 8}$ | F | N/A | $\mathbf{1 . 0 2}$ |

The results of the analysis show that the LOS for the overall intersection and individual movements operate at LOS D or better for the weekday morning peak hour except for the Cone Avenue northwestbound approach, which operates at LOS F. During the weekday afternoon peak hour, the intersection operated at an overall LOS F. In addition, the intersection is overcapacity during the weekday afternoon peak hour with a v/c ratio of 1.02.

To mitigate future traffic growth and future developments, such as the Hall Property, it is recommended that the intersection be reconstructed and realigned. The recommended improvements to the intersection are presented in Figure 2 and are as follows:

- Eliminate the Pomeroy Avenue approach to East Main Street and realign to the east to form a T-intersection with Cone Avenue to the south of East Main Street with Pomeroy Avenue stop-controlled. The realignment will require a full property acquisition at the intersection. In addition, a partial property acquisition adjacent to the full property acquisition may be required.
- Realign the Cone Avenue and Preston Avenue approaches to the east to improve sight distance and turning radii. The realignment may require two partial property acquisitions at the intersection.
- Extend the East Main Street eastbound left turn lane to $230^{\prime}$ 'long.
- Prune vegetation on the south side of East Main Street to improve intersection sight distance from Cone Avenue looking west onto East Main Street.
- Prune vegetation on north side of East Main Street at Preston Avenue to improve intersection sight distance from Preston Avenue looking east onto East Main Street.
- Full traffic signal replacement at the intersection.

An intersection capacity analysis was performed for the recommended reconstructed intersection. The results of the intersection capacity analysis for the 2030 mitigation weekday morning and afternoon peak periods are presented in Table 4. Copies of the Synchro analysis worksheets can be found in Appendix C.

Table 4
2030 Weekday Mitigation Level of Service Analysis - Preston Avenue at East Main Street

|  | Weekday Morning Peak Hour |  |  | Weekday Afternoon Peak Hour |  |  |  |  |
| :--- | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Approach and <br> Movement | Delay <br> (sec) | LOS | Percentile <br> Queue <br> (feet) | v/c <br> Ratio | Delay <br> (sec) | LOS | Percentile <br> Queue <br> (feet) | v/c <br> Ratio |
| East Main St. Eastbound - <br> Left | 8.3 | A | 63 | 0.30 | 17.4 | B | 216 | 0.76 |
| East Main St. Eastbound - <br> Through/Right | 9.1 | A | 132 | 0.33 | 15.4 | B | 391 | 0.65 |
| East Main St. Westbound - <br> Left/Through/Right | 16.7 | B | 199 | 0.47 | 25.2 | C | 266 | 0.56 |
| Preston Ave. Southbound - <br> Left/Through/Right | 45.8 | D | 111 | 0.82 | 37.6 | D | 164 | 0.72 |
| Cone Ave. Northbound - <br> Left/Through/Right | 24.8 | C | 66 | $0 . .56$ | 44.2 | D | 255 | 0.85 |
| Overall | 20.4 | C | N/A | $\mathbf{0 . 6 1}$ | $\mathbf{2 5 . 0}$ | C | N/A | $\mathbf{0 . 7 0}$ |

The results of the analysis show that the LOS for the overall intersection and individual movements operate at LOS D or better for both peak hours In addition, the intersection has additional capacity with the a maximum $\mathrm{v} / \mathrm{c}$ ratio of 0.85 for any individual movement.

The recommended improvements for the remaining portion of Preston Avenue from East Main Street to Parker Road are presented in Figure 3 and are as follows:

- Perform full-depth reconstruction for pavement rehabilitation through entire the section.
- Install bituminous concrete lip curbing on both sides of Preston Avenue.
- Construct concrete sidewalk on west side of Preston Avenue from East Main Street to Parker Road.
- Regrade slope on east side of Preston Avenue at Parker Road to improve intersection sight distance looking south onto Preston Avenue.
- Remove metal beam rail at drop inlet on east side of Preston Avenue, north of East Main Street.
- Install a new closed drainage system from Parker Road to East Main Street. Install 18" outlet pipe on the southwest corner of Preston Avenue and East Main Street where an existing leakoff drains Preston Avenue into a watercourse.
- Install underdrain along the roadway edge on the east side of Preston Avenue from East Main Street to Parker Road.
- Replace all existing signage to conform to latest edition of the Manual of Uniform Traffic Control Devices for reflectivity and letter legend standards.

The construction cost for the recommended improvements for this segment of roadway is $\$ 2,826,000$. A detailed construction cost estimate is presented in Appendix D.

### 5.2 Preston Avenue - Parker Road to Route 66 Off-Ramp

The recommended improvements for Preston Avenue from Parker Road to the Route 66 offramp presented in Figure 3 are as follows:

- Perform full-depth reconstruction for pavement rehabilitation through the entire section.
- CTDOT design standards require a minimum roadway width of $26^{\prime}$ for this classification of roadway. The minimum existing width of roadway through this section is $25^{\prime}$. Depending on the funding source, it may be required to widen the roadway to the CTDOT design standard width of 26 '. The cost of this potential widening has been provided in the cost estimate.
- Construct concrete sidewalk on west side of Preston Avenue from Parker Road to Clearfield Drive.
- Install bituminous concrete lip curbing on both sides of Preston Avenue.
- Prune vegetation on south side of East Main Street to improve intersection sight distance from Pomeroy Avenue and Cone Avenue looking west onto Preston Avenue.
- Prune vegetation on west side of Preston Avenue south of the Route 66 off-ramp to improve intersection sight distance from Clearfield Drive looking north onto Preston Avenue.
- Remove unnecessary portion of metal beam rail at private pull-in area.
- Replace cable guide rail with metal beam rail and proper end treatments at Route 66 offramp.
- Upgrade the existing drainage system with additional catch basins from Parker Road to the Route 66 off-ramp.
- Install underdrain along the roadway edge on the east side of Preston Avenue from Parker Road to the Route 66 off-ramp.
- Replace all existing signage to conform to latest edition of the Manual of Uniform Traffic Control Devices for reflectivity and letter legend standards.

The construction cost for the recommended improvements for this segment of roadway is $\$ 853,000$. A detailed construction cost estimate is presented in Appendix $D$.

### 5.3 Preston Avenue - Route 66 OffRamp to Patton Drive

The recommended improvements for Preston Avenue from the Route 66 off-ramp to Patton Drive presented in Figures 4 and 5 are as follows:

- Mill and overlay Preston Avenue Bridge over Route 66.
- Perform full-depth reconstruction for pavement rehabilitation from Preston Avenue Bridge over Route 66 to Patton Drive.
- CTDOT design standards require a minimum roadway width of $26^{\prime}$ for this classification of roadway. The minimum existing width of roadway through this section is $24^{\prime}$. Depending on the funding source, it may be required to widen the roadway to the CTDOT design standard width of 26 '. The cost of this potential widening has been provided in the cost estimate.
- Install bituminous concrete lip curbing on both sides of Preston Avenue from Preston Avenue Bridge over Route 66 to Patton Drive.
- Prune vegetation on southeast corner of the Preston Avenue at Police Academy Drive to improve intersection sight distance on Police Academy Drive looking south onto Preston Avenue.
- Regrade slope on northeast corner of the Preston Avenue at Police Academy Drive to improve intersection sight distance on Police Academy Drive looking north onto Preston Avenue.
- Clear vegetation on southeast corner of Preston Avenue at Patton Drive to improve intersection sight distance on Patton Drive looking north onto Preston Avenue.
- Replace wire rope rail with metal beam rail and proper end treatment, at northeast corner of Preston Avenue Bridge over Route 66.
- Upgrade metal beam rail end treatment, on the west side of Preston Avenue north of the Route 66 on-ramp.
- Clean scuppers on Preston Avenue Bridge over Route 66.
- Upgrade the existing drainage system with additional catch basins from Route 66 onramp to north of Patton Drive. Upgrade outlet to a 24 " outlet pipe, as necessary.
- Install underdrain along the roadway edge on the east side of Preston Avenue from the Route 66 on-ramp to Patton Drive.
- Replace all existing signage to conform to latest edition of the Manual of Uniform Traffic Control Devices for reflectivity and letter legend standards.

The construction cost for the recommended improvements for this segment of roadway is $\$ 2,386,000$. A detailed construction cost estimate is presented in Appendix D.

### 5.4 Preston Avenue - Patton Drive to Baldwin Avenue

The recommended improvements for Preston Avenue from Patton Drive to Baldwin Avenue presented in Figures 5 and 6 are as follows:

- Perform full-depth reconstruction for pavement rehabilitation through the entire section.
- CTDOT design standards require a minimum roadway width of $26^{\prime}$ for this classification of roadway. The minimum existing width of roadway through this section is $24^{\prime}$. Depending on the funding source, it may be required to widen the roadway to the CTDOT design standard width of 26 '. The cost of this potential widening has been provided in the cost estimate.
- Install bituminous concrete lip curbing on both sides of Preston Avenue.
- Upgrade metal beam rail end treatment on the west side of Preston Avenue north of the Patton Drive.
- Upgrade existing drainage system with additional catch basins from north of Patton Drive to Baldwin Avenue. Upgrade existing outlet to an 18 " pipe, as necessary.
- Install underdrain along the roadway edge on the east side of Preston Avenue from the Patton Drive to Baldwin Avenue.
- Replace all existing signage to conform to latest edition of the Manual of Uniform Traffic Control Devices for reflectivity and letter legend standards.

The construction cost for the recommended improvements for this segment of roadway is $\$ 1,786,000$. A detailed construction cost estimate is presented in Appendix $D$.

### 5.5 Baldwin Avenue - Preston Avenue to Preston Drive

The recommended improvements for Baldwin Avenue from Preston Avenue to Preston Drive presented in Figure 6 are as follows:

- Mill and overlay Baldwin Avenue through the entire section.
- Construct a new 5' wide concrete sidewalk on south side of Baldwin Avenue.
- Install new bituminous concrete lip curbing on both sides of Baldwin Avenue in locations where no curbing exists or existing bituminous concrete lip curbing is damaged.
- Replace wire rope rail with metal beam rail and proper end treatments on north side of Baldwin Avenue between the I-91 off-ramp and Thurrott Avenue.
- Upgrade metal beam rail end treatment on the west side of Preston Avenue north of the I-91 on-ramp.
- Replace all existing signage to conform to latest edition of the Manual of Uniform Traffic Control Devices for reflectivity and letter legend standards.

The construction cost for the recommended improvements for this segment of roadway is $\$ 620,000$. A detailed construction cost estimate is presented in Appendix D.

### 5.6 Baldwin Avenue - Preston Drive to Higby Drive

The recommended improvements for Baldwin Avenue from Preston Drive to Higby Drive presented in Figure 7 are as follows:

- Mill and overlay Baldwin Avenue from Preston Drive to between Heather Heights and Lori Lane
- Perform full-depth reconstruction for pavement rehabilitation and to correct vertical profile deficiencies from between Heather Heights and Lori Lane to Higby Drive. Vertical profile revisions at Heather Heights will result in a maximum cut of 1.5'.
- Construct a new 5' wide concrete sidewalk on south side of Baldwin Avenue from Preston Drive to existing sidewalk between Lori Lane and Heather Heights.
- Reconstruct the existing sidewalk on south side of Baldwin Avenue between Lori Lane and Higby Drive.
- Construct a new 5' wide concrete sidewalk on north side of Baldwin Avenue from trail to Higby Drive.
- Install bituminous concrete lip curbing on both sides of Baldwin Avenue. Install concrete curb where concrete sidewalk borders the roadway.
- Upgrade the existing drainage system with additional catch basins from Preston Drive to Heather Heights. Based on the results of the conceptual drainage analysis, upgrade the existing outlet pipe to 18 ", as necessary.
- Install crosswalk with crosswalk and advanced signage between Higby Drive and Heather Heights to connect reconstructed sidewalk on south side of Baldwin Avenue to proposed sidewalk on north side of Baldwin Avenue.
- Replace all existing signage to conform to latest edition of the Manual of Uniform Traffic Control Devices for reflectivity and letter legend standards.

The construction cost for the recommended improvements for this segment of roadway is $\$ 1,178,000$. A detailed construction cost estimate is presented in Appendix D.

### 5.7 Baldwin Avenue - Higby Drive to Bee Street

The recommended improvements for Baldwin Avenue from Higby Drive to Bee Street presented in Figure 8 are as follows:

- Perform full-depth reconstruction for pavement from Higby Drive to Mattabasset Drive.
- Perform full-depth reconstruction and associated improvements from Mattabasset Drive to west of Winding Brook Lane per the preliminary design plans "Reconstruction of Baldwin Avenue, May 2008".
- Mill and overlay from west of Winding Brook Lane to Bee Street.
- Reconstruct the existing sidewalk on north side of Baldwin Avenue between Higby Drive and Bee Street.
- Install bituminous concrete lip curbing on south side of Baldwin Avenue.
- Install concrete curbing on north side of Baldwin Avenue.
- Prune vegetation on southeast corner of Baldwin Avenue at Bee Street to improve intersection sight distance on Baldwin Avenue looking south onto Baldwin Avenue.
- Upgrade the existing drainage system with additional catch basins from Higby Drive to Winding Brook Lane.
- Upgrade existing drainage system with additional catch basins from Winding Brook Lane to Bee Street.
- Replace all existing signage to conform to latest edition of the Manual of Uniform Traffic Control Devices for reflectivity and letter legend standards.

The construction cost for the recommended improvements for this segment of roadway is $\$ 1,590,000$. A detailed construction cost estimate is presented in Appendix D.

## 6 Implementation of Recommended Improvements and Funding Sources

Based on the recommended improvements and cost estimates prepared for the various roadway segments, the City can prioritize individual projects. A summary of the construction cost for each segment is presented in Table 5.

## Table 5 <br> Construction Cost Summary

| Roadway Segment | Construction Cost |
| :--- | :---: |
| Preston Avenue - East Main Street to Parker Road | $\$ 2,826,000$ |
| Preston Avenue - Parker Road to Route 66 Off-Ramp | $\$ 853,000$ |
| Preston Avenue - Route 66 Off-Ramp to Patton Drive | $\$ 2,386,000$ |
| Preston Avenue - Patton Drive to Baldwin Avenue | $\$ 1,786,000$ |
| Baldwin Avenue - Preston Avenue to Preston Drive | $\$ 620,000$ |
| Baldwin Avenue - Preston Drive to Higby Drive | $\$ 1,178,000$ |
| Baldwin Avenue - Higby Drive to Bee Street | $\$ 1,590,000$ |
| Total | $\$ 11,239,000$ |

The total construction cost for the entire corridor is estimated to be $\$ 11,239,000$
There are various funding sources available for the implementation of the recommended improvements for the corridor, (i.e. Local Capital Improvement (LOCIP), Surface Transportation Plan - Urban (STP-Urban), High Priority Project (HPP), and other State and local funding.)

Short-term improvements such as clearing of vegetation for intersection sight distance improvements, upgrading existing signing, and pavement marking restriping can be implemented in a short-time period at a low cost. Drainage improvements, sidewalk improvements, and milling and overlay can be considered intermediate improvements. Fulldepth reconstruction, vertical profile corrections, and widening can be considered long-term improvement projects, which will require dedicated funding.

The identification of recommended improvements along with construction cost estimates for each roadway segment of the corridor will allow the City to develop a phased improvement plan as funding becomes available.

Figures
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SOUTH CENTRAL REGIONAL COUNCIL OF GOVERNMENTS
PROJECT LOCATION MAP
PRESTON AVENUE/BALDWIN AVENUE CORRIDOR STUDY

MERIDEN CONNECTICUT

PROJ. No: 20090602A10 DATE: JUNE 2010

FIG. 1


Figure 2 - Preston Avenue East Main Street Intersection Improvements (Alternative \#1)

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South Central Regional Council of Governments
CORRIDOR STUDY MERIDEN, CONNECTICUT



LEGEND
FULL-DEPTH RECONSTRUCTION FOR PAVEMENT REHABILITATION.

INSTALL UNDERDRAIN


LIMITED SIGHT DISTANCE LOOKING LEFT PRESTON AVE. AT PARKER ROAD LOOKING NORTH

NOTES

- REPLACE ALL EXISTING SIGNING TO CONFORM TO LATEST EDITION OF MUTCD
- ROADWAY MAY REQUIRE WIDENING TO 26' WIDE DEPENDING ON FUNDING SOURCE


REPLACE OBSOLETE CABLE GUIDE RAIL PRESTON AVE. AT ROUTE 66 OFF-RAMP

Figure 4 - Preston Avenue
From East Main St to Rte 66 Off-Ramp

146 HARTFORD RD

FUSS \& O'NEILL
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MANCHESTER, CT 06040

South Central Regional Council of Governments
CORRIDOR STUDY
MERIDEN, CONNECTICUT



REPLACE OBSOLETE WIRE ROPE RAIL PRESTON AVE. OVER ROUTE 66

LEGEND
FULL-DEPTH RECONSTRUCTION FOR PAVEMENT REHABILITATION.

MILL AND OVERLAY
INSTALL UNDERDRAIN


PRUNE VEGETATION TO IMPROVE SIGHT DISTANCE JOHNSON AVE. AT POLICE ACADEMY DR. LOOKING SOUTH

NOTES

- REPLACE ALL EXISTING SIGNING TO CONFORM TO LATEST EDITION OF MUTCD
- ROADWAY MAY REQUIRE WIDENING TO 26' WIDE DEPENDING ON FUNDING SOURCE


REGRADE SLOPE FOR POLICE ACADEMY DRIVE PRESTON AVENUE LOOKING EAST TOWARDS ROUTE 66

South Central Regional Council of Governments
FUSS \& O'NEILL
Disciplines to Deliver
WANCHESTER CT 06040

CORRIDOR STUDY
MERIDEN, CONNECTICUT
June 2010


REMOVE VEGETATION TO IMPROVE SIGHT DISTANCE PRESTON AVE. AT PATTON DR. LOOKING SOUTH

LEGEND
FULL-DEPTH RECONSTRUCTION FOR PAVEMENT REHABILITATION. VARIABLE WIDTH WIDENING TO PROVIDE 24' WIDE MINIMUM ROADWAY.

REMOVE OBSTRUCTIONS FROM SIGHT TRIANGLES
-------- INSTALL UNDERDRAIN


POTENTIALLY WIDEN ROADWAY TO ${ }^{\prime} 6^{\prime}$ PRESTON AVE. AT PATTON DR. LOOKING EAST

NOTES

- REPLACE ALL EXISTING SIGNING TO CONFORM TO LATEST EDITION OF MUTCD
- ROADWAY MAY REQUIRE WIDENING TO 26' WIDE DEPENDING ON FUNDING SOURCE


POTENTIALLY WIDEN ROADWAY TO 26' PRESTON AVE. EAST OF PATTON DR.

Figure 6 - Preston Avenue
From North of Route 66 OnRamp to South of Baldwin Ave

South Central Regional Council of Governments

CORRIDOR STUDY
MERIDEN, CONNECTICUT



LEGEND
FULL-DEPTH RECONSTRUCTION FOR PAVEMENT REHABILITATION. VARIABLE WIDTH WIDENING TO PROVIDE 24 ' WIDE MINIMUM ROADWAY.

MILL AND OVERLAY WITH SIDEWALK EXTENSION FROM OFFICE PARK TO THE NORTH.


SUBSTANDARD VERTICAL CLEARANCE UNDER I-91 baldwin avenue Looking west under I-91

UPGRADE ROADSIDE PROTECTION AT CULVERT JOHNSON AVE. AT FAIRFAX AVE. LOOKING EAST

NOTES

- REPLACE ALL EXISTING SIGNING TO CONFORM TO LATEST EDITION OF MUTCD
- ROADWAY MAY REQUIRE WIDENING TO 26' WIDE DEPENDING ON FUNDING SOURCE


MILL AND OVERLAY EXISTING PAVEMENT BALDWIN AVE. AT PRESTON DR. LOOKING WEST

Figure 7 - Preston Avenue/Baldwin Avenue South of Baldwin Ave to Preston Drive

South Central Regional Council of Governments

CORRIDOR STUDY MERIDEN, CONNECTICUT




RECONSTRUCT ROADWAY TO IMPROVE SIGHT DISTANCE BALDWIN AVE. AT MATTABASSET DR. LOOKING WEST

FULL-DEPTH RECONSTRUCTION FOR PAVEMENT REHABILITATION. VARIABLE WIDTH WIDENING TO PROVIDE 24' WIDE MINIMUM ROADWAY. RECONSTRUCT EXISTING SIDEWALKS WITH CONCRETE SIDEWALKS AND ADA COMPLIANT RAMPS.

FULL-DEPTH RECONSTRUCTION AND ASSOCIATED IMPROVEMENTS PER BALDWIN AVENUE IMPROVEMENTS PRELIMINARY DESIGN PLANS.

MILL AND OVERLAY. VARIABLE WIDTH WIDENING TO PROVIDE 24' WIDE MINIMUM ROADWAY. RECONSTRUCT EXISTING SIDEWALKS WITH CONCRETE SIDEWALKS AND ADA COMPLIANT RAMPS.

Figure 9 - Baldwin Avenue From Higby Drive to Bee Street

## WTVM/WMW

FULL-DEPTH RECONSTRUCTION TO CORRECT VERTICAL PROFILE DEFICIENCIES

## NOTES

- REPLACE ALL EXISTING SIGNING TO CONFORM TO LATEST EDITION OF MUTCD


PRUNE VEGETATION TO IMPROVE SIGHT DISTANCE BEE ST. AT BALDWIN AVE. LOOKING SOUTH

South Central Regional Council of Governments
CORRIDOR STUDY
MERIDEN, CONNECTICUT

June 2010

Traffic Counts

Latitude: $0^{\prime} 0.000$ Undefined

| Start | 07-Jun-10 |  | Tue |  | Wed |  | Thu |  | Fri |  | Sat |  | Sun |  | Week Average |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Time | Northbound | Southbo | Northbo | Southbo | Northbo | Southbo | Northbo | Southbo | Northbo | Southbo | Northbo | Southbo | Northbo | Southbo | Northbo | Southbo |
| 12:00 AM | , | * | , | * | * | * | * | - | 18 | 12 | 21 | 17 | 12 | 21 | 17 | 17 |
| 01:00 | * | * | * | * | * | * | * | * | 8 | 4 | 15 | 8 | 16 | 11 | 13 | 8 |
| 02:00 | * | * | * | * | * | * | * | * | 8 | 5 | 15 | 10 | 18 | 14 | 14 | 10 |
| 03:00 | * | * | * | * | * | * | * | * | 6 | 5 | 6 | 9 | 4 | 6 | 5 | 7 |
| 04:00 | * | * | * | * | * | * | * | * | 10 | 14 | 7 | 9 | 3 | 6 | 7 | 10 |
| 05:00 | * | * | * | * | * | * | * | * | 10 | 42 | 6 | 17 | 5 | 8 | 7 | 22 |
| 06:00 | * | * | * | * | * | * | * | * | 40 | 104 | 22 | 50 | 15 | 20 | 26 | 58 |
| 07:00 | * | * | * | * | * | * | * | * | 84 | 225 | 27 | 57 | 28 | 38 | 46 | 107 |
| 08:00 | * | * | * | * | * | * | * | * | 72 | 189 | 44 | 79 | 39 | 45 | 52 | 104 |
| 09:00 | * | * | * | * | * | * | * | * | 60 | 111 | 68 | 118 | 37 | 83 | 55 | 104 |
| 10:00 | * | * | * | * | * | * | * | * | 54 | 88 | 88 | 121 | 63 | 132 | 68 | 114 |
| 11:00 | * | * | * | * | * | * | 81 | 108 | 82 | 123 | 92 | 133 | 80 | 96 | 84 | 115 |
| 12:00 PM | * | * | * | * | * | * | 89 | 126 | 91 | 121 | 93 | 131 | 88 | 128 | 90 | 126 |
| 01:00 | * | * | * | * | * | * | 97 | 103 | 109 | 122 | 95 | 127 | 78 | 117 | 95 | 117 |
| 02:00 | * | * | * | * | * | * | 123 | 102 | 128 | 140 | 102 | 102 | 93 | 123 | 112 | 117 |
| 03:00 | * | * | * | * | * | * | 149 | 159 | 153 | 157 | 81 | 103 | 86 | 87 | 117 | 126 |
| 04:00 | * | * | * | * | * | * | 203 | 150 | 193 | 198 | 102 | 116 | 64 | 116 | 140 | 145 |
| 05:00 | * | * | * | * | * | * | 205 | 228 | 191 | 194 | 94 | 107 | 74 | 90 | 141 | 155 |
| 06:00 | * | * | * | * | * | * | 126 | 137 | 105 | 149 | 70 | 100 | 73 | 62 | 94 | 112 |
| 07:00 | * | * | * | * | * | * | 92 | 75 | 115 | 104 | 72 | 88 | 59 | 74 | 84 | 85 |
| 08:00 | * | * | * | * | * | * | 94 | 58 | 87 | 79 | 57 | 57 | 44 | 56 | 70 | 62 |
| 09:00 | * | * | * | * | * | * | 53 | 52 | 44 | 64 | 51 | 63 | 32 | 46 | 45 | 56 |
| 10:00 | * | * | * | * | * | * | 30 | 24 | 32 | 40 | 39 | 41 | 15 | 28 | 29 | 33 |
| 11:00 | * | * | * | * | * | * | 33 | 32 | 40 | 42 | 30 | 29 | 12 | 19 | 29 | 30 |
| Lane | 0 | 0 | 0 | 0 | 0 | 0 | 1375 | 1354 | 1740 | 2332 | 1297 | 1692 | 1038 | 1426 | $1440$ | 1840 |
| Day | 0 |  | 0 |  | 0 |  | 27 |  | 407 |  | 298 |  | 24 |  | $328$ |  |
| AM Peak |  |  |  |  |  |  | 11:00 | 11:00 | 07:00 | 07:00 | 11:00 | 11:00 | 11:00 | 10:00 | 11:00 | 11:00 |
| Vol. |  |  |  |  |  |  | 81 | 108 | 84 | 225 | 92 | 133 | 80 | 132 | 84 | 115 |
| PM Peak |  |  |  |  |  |  | 17:00 | 17:00 | 16:00 | 16:00 | 14:00 | 12:00 | 14:00 | 12:00 | 17:00 | 17:00 |
| Vol. |  |  |  |  |  |  | 205 | 228 | 193 | 198 | 102 | 131 | 93 | 128 | 141 | 155 |

Preston Avenue South of I-91 Ramps Meriden, Connecticut

63 Sugar Maple Lane
Kensington, Connecticut 06037

Site Code: 2205 Station ID:

Latitude: 0 ' 0.000 Undefined


# Connecticut Counts LLC 

63 Sugar Maple Lane

Preston Avenue South of I-91 Ramps Meriden, Connecticut

Kensington, Connecticut 06037
(860) 828-1693


Preston Avenue South of I-91 Ramps Meriden, Connecticut

Connecticut Counts LLC
63 Sugar Maple Lane
Kensington, Connecticut 06037
(860) 828-1693

Page 2

Site Code: 2205 Station ID:

| Northbound |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Latitude: 0' 0.000 Undefined |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 0 | 16 | 21 | 26 | 31 | 36 | 41 | 46 | 51 | 56 | 61 | 66 | 71 | 76 |  | Pace | Number |
| Time | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 9999 | Total | Speed | in Pace |
| 6/11/10 | 0 | 0 | 0 | 2 | 4 | 6 | 3 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 18 | 29-38 | 10 |
| 01:00 | 0 | 0 | 0 | 0 | 3 | 3 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 33-42 | 8 |
| 02:00 | 0 | 0 | 0 | 1 | 1 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 32-41 | 7 |
| 03:00 | 0 | 0 | 0 | 0 | 0 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 32-41 | 6 |
| 04:00 | 0 | 1 | 0 | 1 | 1 | 2 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 35-44 | 7 |
| 05:00 | 0 | 0 | 0 | 0 | 1 | 3 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 10 | 38-47 | 9 |
| 06:00 | 0 | 0 | 0 | 0 | 4 | 14 | 16 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 40 | 36-45 | 30 |
| 07:00 | 0 | 0 | 0 | 2 | 6 | 29 | 38 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 84 | 36-45 | 67 |
| 08:00 | 0 | 0 | 0 | 1 | 8 | 35 | 24 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 72 | 36-45 | 59 |
| 09:00 | 0 | 0 | 0 | 4 | 12 | 22 | 18 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 60 | 34-43 | 40 |
| 10:00 | 1 | 0 | 0 | 3 | 13 | 19 | 17 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 54 | 33-42 | 36 |
| 11:00 | 0 | 0 | 1 | 3 | 16 | 28 | 28 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 82 | 36-45 | 56 |
| 12 PM | 0 | 0 | 0 | 6 | 13 | 35 | 30 | 6 | 1 | 0 | 0 | 0 | 0 | 0 | 91 | 36-45 | 65 |
| 13:00 | 0 | 0 | 0 | 7 | 18 | 36 | 35 | 10 | 3 | 0 | 0 | 0 | 0 | 0 | 109 | 36-45 | 71 |
| 14:00 | 1 | 1 | 4 | 8 | 20 | 52 | 31 | 10 | 1 | 0 | 0 | 0 | 0 | 0 | 128 | 36-45 | 83 |
| 15:00 | 0 | 0 | 0 | 5 | 15 | 72 | 51 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 153 | 36-45 | 123 |
| 16:00 | 1 | 0 | 0 | 2 | 10 | 85 | 80 | 14 | 0 | 0 | 1 | 0 | 0 | 0 | 193 | 36-45 | 165 |
| 17:00 | 0 | 0 | 0 | 6 | 14 | 87 | 71 | 11 | 0 | 0 | 0 | 0 | 1 | 1 | 191 | 36-45 | 158 |
| 18:00 | 0 | 0 | 1 | 2 | 3 | 49 | 40 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 105 | 36-45 | 89 |
| 19:00 | 0 | 0 | 0 | 1 | 20 | 43 | 41 | 6 | 4 | 0 | 0 | 0 | 0 | 0 | 115 | 36-45 | 84 |
| 20:00 | 0 | 0 | 0 | 2 | 20 | 27 | 33 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 87 | 36-45 | 60 |
| 21:00 | 0 | 0 | 0 | 1 | 10 | 17 | 12 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 33-42 | 29 |
| 22:00 | 0 | 0 | 0 | 0 | 9 | 18 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 32 | 31-40 | 27 |
| 23:00 | 0 | 0 | 0 | 6 | 8 | 17 | 1 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 40 | $31-40$ | 25 |
| Total | 3 | 2 | 6 | 63 | 229 | 709 | 585 | 125 | 15 | 0 | 1 | 0 | 1 | 1 | 1740 |  |  |
| Percent | 0.2\% | 0.1\% | 0.3\% | 3.6\% | 13.2\% | 40.7\% | 33.6\% | 7.2\% | 0.9\% | 0.0\% | 0.1\% | 0.0\% | 0.1\% | 0.1\% |  |  |  |
| AM Peak | 10:00 | 04:00 | 11:00 | 09:00 | 11:00 | 08:00 | 07:00 | 07:00 | 06:00 |  |  |  |  |  | 07:00 |  |  |
| Vol. | 1 | 1 | 1 | 4 | 16 | 35 | 38 | 9 | 1 |  |  |  |  |  | 84 |  |  |
| PM Peak | 14:00 | 14:00 | 14:00 | 14:00 | 14:00 | 17:00 | 16:00 | 16:00 | 19:00 |  | 16:00 |  | 17:00 | 17:00 | 16:00 |  |  |
| Vol. | 1 | 1 | 4 | 8 | 20 | 87 | 80 | 14 | 4 |  | 1 |  | 1 | 1 | 193 |  |  |

63 Sugar Maple Lane
Kensington, Connecticut 06037
(860) 828-1693

|  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 0 | 16 | 21 | 26 | 31 | 36 | 41 | 46 | 51 | 56 | 61 | 66 | 71 | 76 |  | Pace | Number |
| Time | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 9999 | Total | Speed | in Pace |
| 6/12/10 | 0 | 0 | 0 | 4 | 3 | 9 | 2 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 21 | 33-42 | 14 |
| 01:00 | 0 | 0 | 0 | 0 | 2 | 5 | 6 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 15 | 34-43 | 11 |
| 02:00 | 0 | 0 | 0 | 1 | 6 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 30-39 | 12 |
| 03:00 | 0 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 6 | 37-46 | 5 |
| 04:00 | 0 | 1 | 0 | 0 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | 28-37 | 5 |
| 05:00 | 0 | 0 | 0 | 0 | 2 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 28-37 | 4 |
| 06:00 | 0 | 0 | 0 | 0 | 4 | 3 | 9 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 22 | 38-47 | 14 |
| 07:00 | 0 | 0 | 0 | 0 | 5 | 9 | 9 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 27 | 35-44 | 18 |
| 08:00 | 0 | 0 | 0 | 2 | 10 | 17 | 10 | 3 | 0 | 2 | 0 | 0 | 0 | 0 | 44 | 31-40 | 27 |
| 09:00 | 0 | 1 | 1 | 2 | 11 | 26 | 24 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 68 | 36-45 | 50 |
| 10:00 | 1 | 1 | 0 | 4 | 16 | 24 | 31 | 8 | 3 | 0 | 0 | 0 | 0 | 0 | 88 | 36-45 | 55 |
| 11:00 | 0 | 0 | 0 | 5 | 10 | 35 | 33 | 7 | 1 | 0 | 1 | 0 | 0 | 0 | 92 | 36-45 | 68 |
| 12 PM | 0 | 0 | 0 | 3 | 17 | 41 | 26 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 93 | 36-45 | 67 |
| 13:00 | 0 | 0 | 0 | 3 | 18 | 41 | 23 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 95 | 34-43 | 64 |
| 14:00 | 0 | 0 | 0 | 2 | 17 | 38 | 35 | 9 | 0 | 0 | 1 | 0 | 0 | 0 | 102 | 36-45 | 73 |
| 15:00 | 0 | 0 | 0 | 0 | 8 | 38 | 21 | 11 | 2 | 1 | 0 | 0 | 0 | 0 | 81 | 36-45 | 59 |
| 16:00 | 0 | 1 | 0 | 2 | 7 | 37 | 41 | 13 | 0 | 0 | 0 | 0 | 0 | 1 | 102 | 36-45 | 78 |
| 17:00 | 0 | 0 | 0 | 1 | 7 | 32 | 38 | 13 | 3 | 0 | 0 | 0 | 0 | 0 | 94 | 36-45 | 70 |
| 18:00 | 0 | 0 | 0 | 2 | 6 | 27 | 27 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 70 | 36-45 | 54 |
| 19:00 | 0 | 0 | 1 | 2 | 11 | 34 | 20 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 72 | 36-45 | 54 |
| 20:00 | 0 | 0 | 0 | 8 | 8 | 26 | 13 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 57 | 34-43 | 39 |
| 21:00 | 0 | 0 | 1 | 6 | 16 | 20 | 5 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 51 | 31-40 | 36 |
| 22:00 | 0 | 0 | 0 | 9 | 13 | 11 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 39 | 27-36 | 24 |
| 23:00 | 0 | 1 | 0 | 4 | 7 | 8 | 4 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 30 | 29-38 | 15 |
| Total | 1 | 5 | 3 | 60 | 207 | 493 | 389 | 114 | 17 | 5 | 2 | 0 | 0 | 1 | 1297 |  |  |
| Percent | 0.1\% | 0.4\% | 0.2\% | 4.6\% | 16.0\% | 38.0\% | 30.0\% | 8.8\% | 1.3\% | 0.4\% | 0.2\% | 0.0\% | 0.0\% | 0.1\% |  |  |  |
| AM Peak | 10:00 | 04:00 | 09:00 | 11:00 | 10:00 | 11:00 | 11:00 | 10:00 | 10:00 | 08:00 | 11:00 |  |  |  | 11:00 |  |  |
| Vol. | 1 | 1 | 1 | 5 | 16 | 35 | 33 | 8 | 3 | 2 | 1 |  |  |  | 92 |  |  |
| PM Peak |  | 16:00 | 19:00 | 22:00 | 13:00 | 12:00 | 16:00 | 16:00 | 17:00 | 15:00 | 14:00 |  |  | 16:00 | 14:00 |  |  |
| Vol. |  | 1 | 1 | 9 | 18 | 41 | 41 | 13 | 3 | 1 | 1 |  |  | 1 | 102 |  |  |

Connecticut Counts LLC
63 Sugar Maple Lane
Kensington, Connecticut 06037
(860) 828-1693

| Northbound |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Latitude: $0^{\prime} 0.000$ Undefined |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 0 | 16 | 21 | 26 | 31 | 36 | 41 | 46 | 51 | 56 | 61 | 66 | 71 | 76 |  | Pace | Number |
| Time | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 9999 | Total | Speed | in Pace |
| 6/13/10 | 0 | 0 | 0 | 0 | 4 | 6 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 31-40 | 10 |
| 01:00 | 0 | 0 | 0 | 0 | 3 | 10 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 16 | 33-42 | 15 |
| 02:00 | 0 | 0 | 0 | 1 | 3 | 8 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 18 | 33-42 | 13 |
| 03:00 | 0 | 0 | 0 | 0 | 1 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 32-41 | 4 |
| 04:00 | 0 | 0 | 0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 28-37 | 3 |
| 05:00 | 1 | 0 | 0 | 1 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 33-42 | 3 |
| 06:00 | 0 | 0 | 0 | 2 | 1 | 2 | 6 | 2 | 1 | 1 | 0 | 0 | 0 | 0 | 15 | 38-47 | 10 |
| 07:00 | 0 | 0 | 0 | 0 | 6 | 12 | 9 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 28 | 35-44 | 22 |
| 08:00 | 0 | 0 | 0 | 3 | 5 | 20 | 7 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 39 | 33-42 | 27 |
| 09:00 | 0 | 1 | 1 | 3 | 3 | 14 | 13 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 37 | 36-45 | 27 |
| 10:00 | 0 | 0 | 0 | 1 | 5 | 28 | 23 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 63 | 36-45 | 51 |
| 11:00 | 0 | 0 | 0 | 5 | 6 | 34 | 29 | 5 | 0 | 1 | 0 | 0 | 0 | 0 | 80 | 36-45 | 63 |
| 12 PM | 0 | 0 | 0 | 4 | 11 | 34 | 29 | 7 | 1 | 2 | 0 | 0 | 0 | 0 | 88 | 36-45 | 63 |
| 13:00 | 0 | 1 | 1 | 3 | 14 | 32 | 24 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 78 | 36-45 | 56 |
| 14:00 | 0 | 0 | 0 | 0 | 6 | 55 | 24 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 93 | 36-45 | 79 |
| 15:00 | 0 | 0 | 0 | 2 | 29 | 25 | 24 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 86 | 31-40 | 54 |
| 16:00 | 0 | 0 | 0 | 1 | 7 | 32 | 19 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 64 | 36-45 | 51 |
| 17:00 | 0 | 0 | 2 | 2 | 7 | 25 | 33 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 74 | 36-45 | 58 |
| 18:00 | 1 | 0 | 0 | 1 | 13 | 29 | 22 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 73 | 36-45 | 51 |
| 19:00 | 0 | 1 | 2 | 0 | 8 | 22 | 18 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 59 | 36-45 | 40 |
| 20:00 | 0 | 0 | 0 | 2 | 6 | 20 | 13 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 44 | 35-44 | 33 |
| 21:00 | 0 | 0 | 0 | 0 | 8 | 16 | 6 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 32 | 32-41 | 25 |
| 22:00 | 0 | 0 | 0 | 0 | 3 | 6 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 33-42 | 11 |
| 23:00 | 0 | 0 | 0 | 1 | 3 | 4 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 30-39 | 8 |
| Total | 2 | 3 | 6 | 32 | 153 | 439 | 316 | 72 | 10 | 5 | 0 | 0 | 0 | 0 | 1038 |  |  |
| Percent | 0.2\% | 0.3\% | 0.6\% | 3.1\% | 14.7\% | 42.3\% | 30.4\% | 6.9\% | 1.0\% | 0.5\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak | 05:00 | 09:00 | 09:00 | 11:00 | 07:00 | 11:00 | 11:00 | 11:00 | 10:00 | 02:00 |  |  |  |  | 11:00 |  |  |
| Vol. | 1 | 1 | 1 | 5 | 6 | 34 | 29 | 5 | 2 | 1 |  |  |  |  | 80 |  |  |
| PM Peak | 18:00 | 13:00 | 17:00 | 12:00 | 15:00 | 14:00 | 17:00 | 12:00 | 19:00 | 12:00 |  |  |  |  | 14:00 |  |  |
| Vol. | 1 | 1 | 2 | 4 | 29 | 55 | 33 | 7 | 2 | 2 |  |  |  |  | 93 |  |  |

63 Sugar Maple Lane
Kensington, Connecticut 06037
(860) 828-1693

Site Code: 2205 Station ID:

| Northbound |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Latitude: 0 ' 0.000 Undefined |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 0 | 16 | 21 | 26 | 31 | 36 | 41 | 46 | 51 | 56 | 61 | 66 | 71 | 76 |  | Pace | Number |
| Time | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 9999 | Total | Speed | in Pace |
| 6/14/10 | 0 | 0 | 0 | 1 | 2 | 3 | 1 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 9 | 29-38 | 6 |
| 01:00 | 0 | 0 | 0 | 1 | 0 | 3 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 29-38 | 3 |
| 02:00 | 0 | 0 | 0 | 0 | 0 | 4 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 32-41 | 5 |
| 03:00 | 0 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 32-41 | 2 |
| 04:00 | 0 | 1 | 0 | 0 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 7-16 | 1 |
| 05:00 | 0 | 0 | 0 | 0 | 3 | 6 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 33-42 | 11 |
| 06:00 | 0 | 0 | 0 | 0 | 2 | 12 | 11 | 5 | 2 | 0 | 0 | 0 | 0 | 0 | 32 | 36-45 | 23 |
| 07:00 | 0 | 0 | 1 | 5 | 18 | 39 | 37 | 5 | 1 | 0 | 0 | 0 | 0 | 0 | 106 | 36-45 | 76 |
| 08:00 | 0 | 0 | 3 | 3 | 12 | 30 | 23 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 76 | 36-45 | 53 |
| 09:00 | 0 | 0 | 1 | 1 | 9 | 18 | 16 | 7 | 1 | 0 | 0 | 0 | 0 | 0 | 53 | 36-45 | 34 |
| 10:00 | 0 | 0 | 1 | 4 | 15 | 23 | 15 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 61 | $31-40$ | 38 |
| 11:00 | 1 | 0 | 1 | 3 | 10 | 23 | 16 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 60 | 36-45 | 39 |
| 12 PM | 1 | 0 | 3 | 1 | 16 | 53 | 25 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 103 | 36-45 | 78 |
| 13:00 | 0 | 0 | 1 | 7 | 10 | 38 | 32 | 5 | 2 | 2 | 0 | 0 | 0 | 0 | 97 | 36-45 | 70 |
| 14:00 | 0 | 1 | 1 | 2 | 22 | 42 | 28 | 7 | 0 | 1 | 0 | 0 | 0 | 0 | 104 | 34-43 | 70 |
| 15:00 | 2 | 0 | 0 | 4 | 14 | 54 | 47 | 13 | 0 | 0 | 0 | 0 | 0 | 0 | 134 | 36-45 | 101 |
| 16:00 | 0 | 2 | 0 | 5 | 23 | 83 | 67 | 15 | 2 | 0 | 0 | 0 | 0 | 0 | 197 | 36-45 | 150 |
| 17:00 | 1 | 0 | 0 | 2 | 33 | 89 | 87 | 12 | 0 | 0 | 0 | 0 | 0 | 0 | 224 | 36-45 | 176 |
| 18:00 | 0 | 0 | 0 | 3 | 13 | 35 | 29 | 12 | 1 | 1 | 0 | 0 | 0 | 0 | 94 | 36-45 | 64 |
| 19:00 | 0 | 0 | 0 | 3 | 12 | 31 | 36 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 88 | 36-45 | 67 |
| 20:00 | 0 | 0 | 0 | 3 | 15 | 34 | 27 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 82 | 36-45 | 61 |
| 21:00 | 0 | 0 | 0 | 8 | 15 | 15 | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 47 | 31-40 | 30 |
| 22:00 | 0 | 0 | 0 | 0 | 5 | 14 | 13 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 35 | 36-45 | 27 |
| 23:00 | 0 | 0 | 0 | 0 | 3 | 6 | 4 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 17 | 33-42 | 11 |
| Total | 5 | 4 | 12 | 56 | 253 | 656 | 531 | 116 | 11 | 5 | 0 | 0 | 0 | 0 | 1649 |  |  |
| Percent | 0.3\% | 0.2\% | 0.7\% | 3.4\% | 15.3\% | 39.8\% | 32.2\% | 7.0\% | 0.7\% | 0.3\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak | 11:00 | 04:00 | 08:00 | 07:00 | 07:00 | 07:00 | 07:00 | 09:00 | 06:00 | 00:00 |  |  |  |  | 07:00 |  |  |
| Vol. | 1 | 1 | 3 | 5 | 18 | 39 | 37 | 7 | 2 | 1 |  |  |  |  | 106 |  |  |
| PM Peak | 15:00 | 16:00 | 12:00 | 21:00 | 17:00 | 17:00 | 17:00 | 16:00 | 13:00 | 13:00 |  |  |  |  | 17:00 |  |  |
| Vol. | 2 | 2 | 3 | 8 | 33 | 89 | 87 | 15 | 2 | 2 |  |  |  |  | 224 |  |  |

Preston Avenue South of I-91 Ramps
Meriden, Connecticut


# Connecticut Counts LLC 

Page 7

Preston Avenue South of I-91 Ramps Meriden, Connecticut

63 Sugar Maple Lane
Kensington, Connecticut 06037



Site Code: 2205 Station ID:

Latitude: $0^{\prime} 0.000$ Undefined -

# Connecticut Counts LLC <br> 63 Sugar Maple Lane <br> Kensington, Connecticut 06037 <br> (860) 828-1693 

Page 8

Preston Avenue South of I-91 Ramps Meriden, Connecticut

| Southbound |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Latitud | 0' 0.000 | Undefined |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 0 | 16 | 21 | 26 | 31 | 36 | 41 | 46 | 51 | 56 | 61 | 66 | 71 | 76 |  | Pace | Number |
| Time | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 9999 | Total | Speed | in Pace |
| 6/11/10 | 0 | 0 | 1 | 0 | 1 | 6 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 12 | 34-43 | 10 |
| 01:00 | 0 | 0 | 0 | 0 | 2 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 23-32 | 2 |
| 02:00 | 0 | 0 | 0 | 0 | 1 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 34-43 | 5 |
| 03:00 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 42-51 | 3 |
| 04:00 | 0 | 0 | 0 | 0 | 3 | 2 | 3 | 3 | 2 | 0 | 0 | 0 | 1 | 0 | 14 | 39-48 | 8 |
| 05:00 | 0 | 0 | 0 | 1 | 1 | 12 | 18 | 8 | 2 | 0 | 0 | 0 | 0 | 0 | 42 | 36-45 | 30 |
| 06:00 | 0 | 0 | 0 | 0 | 4 | 24 | 56 | 18 | 2 | 0 | 0 | 0 | 0 | 0 | 104 | 36-45 | 80 |
| 07:00 | 0 | 0 | 0 | 3 | 12 | 58 | 103 | 44 | 5 | 0 | 0 | 0 | 0 | 0 | 225 | 36-45 | 161 |
| 08:00 | 0 | 1 | 1 | 1 | 7 | 57 | 86 | 25 | 9 | 2 | 0 | 0 | 0 | 0 | 189 | 36-45 | 143 |
| 09:00 | 0 | 0 | 0 | 1 | 10 | 44 | 36 | 17 | 2 | 1 | 0 | 0 | 0 | 0 | 111 | 36-45 | 80 |
| 10:00 | 0 | 0 | 0 | 1 | 3 | 28 | 33 | 16 | 7 | 0 | 0 | 0 | 0 | 0 | 88 | 36-45 | 61 |
| 11:00 | 0 | 0 | 4 | 6 | 9 | 35 | 50 | 16 | 3 | 0 | 0 | 0 | 0 | 0 | 123 | 36-45 | 85 |
| 12 PM | 2 | 0 | 0 | 1 | 12 | 39 | 46 | 18 | 3 | 0 | 0 | 0 | 0 | 0 | 121 | 36-45 | 85 |
| 13:00 | 0 | 0 | 0 | 1 | 18 | 34 | 40 | 25 | 3 | 1 | 0 | 0 | 0 | 0 | 122 | 36-45 | 74 |
| 14:00 | 0 | 0 | 0 | 2 | 16 | 36 | 58 | 21 | 6 | 1 | 0 | 0 | 0 | 0 | 140 | 36-45 | 94 |
| 15:00 | 0 | 0 | 0 | 0 | 5 | 41 | 75 | 32 | 2 | 2 | 0 | 0 | 0 | 0 | 157 | 36-45 | 116 |
| 16:00 | 1 | 1 | 1 | 1 | 7 | 61 | 101 | 21 | 3 | 1 | 0 | 0 | 0 | 0 | 198 | 36-45 | 162 |
| 17:00 | 0 | 0 | 1 | 1 | 16 | 54 | 84 | 30 | 6 | 1 | 1 | 0 | 0 | 0 | 194 | 36-45 | 138 |
| 18:00 | 0 | 1 | 1 | 1 | 13 | 40 | 72 | 18 | 3 | 0 | 0 | 0 | 0 | 0 | 149 | 36-45 | 112 |
| 19:00 | 0 | 0 | 0 | 0 | 5 | 26 | 46 | 20 | 6 | 1 | 0 | 0 | 0 | 0 | 104 | 36-45 | 72 |
| 20:00 | 1 | 0 | 0 | 0 | 6 | 19 | 36 | 12 | 3 | 2 | 0 | 0 | 0 | 0 | 79 | 36-45 | 55 |
| 21:00 | 0 | 0 | 0 | 1 | 4 | 28 | 23 | 5 | 3 | 0 | 0 | 0 | 0 | 0 | 64 | 36-45 | 51 |
| 22:00 | 0 | 0 | 0 | 0 | 4 | 14 | 15 | 4 | 2 | 1 | 0 | 0 | 0 | 0 | 40 | 36-45 | 29 |
| 23:00 | 0 | 0 | 2 | 2 | 8 | 10 | 15 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 42 | 36-45 | 25 |
| Total | 4 | 3 | 11 | 23 | 168 | 670 | 1004 | 361 | 73 | 13 | 1 | 0 | 1 | 0 | 2332 |  |  |
| Percent | 0.2\% | 0.1\% | 0.5\% | 1.0\% | 7.2\% | 28.7\% | 43.1\% | 15.5\% | 3.1\% | 0.6\% | 0.0\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak |  | 08:00 | 11:00 | 11:00 | 07:00 | 07:00 | 07:00 | 07:00 | 08:00 | 08:00 |  |  | 04:00 |  | 07:00 |  |  |
| Vol. |  | 1 | 4 | 6 | 12 | 58 | 103 | 44 | 9 | 2 |  |  | 1 |  | 225 |  |  |
| PM Peak | 12:00 | 16:00 | 23:00 | 14:00 | 13:00 | 16:00 | 16:00 | 15:00 | 14:00 | 15:00 | 17:00 |  |  |  | 16:00 |  |  |
| Vol. | 2 | 1 | 2 | 2 | 18 | 61 | 101 | 32 | 6 | 2 | 1 |  |  |  | 198 |  |  |


| Southbound |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Latitude: $0^{\prime} 0.000$ Undefined |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 0 | 16 | 21 | 26 | 31 | 36 | 41 | 46 | 51 | 56 | 61 | 66 | 71 | 76 |  | Pace | Number |
| Time | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 9999 | Total | Speed | in Pace |
| 6/12/10 | 0 | 0 | 0 | 1 | 1 | 3 | 7 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 38-47 | 12 |
| 01:00 | 0 | 0 | 0 | 0 | 1 | 2 | 3 | 1 | 0 | 0 | 1 | 0 | 0 | 0 | 8 | 34-43 | 6 |
| 02:00 | 0 | 0 | 0 | 1 | 0 | 4 | 2 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 10 | 36-45 | 6 |
| 03:00 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 3 | 1 | 0 | 0 | 0 | 0 | 0 | 9 | 39-48 | 8 |
| 04:00 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 1 | 3 | 0 | 0 | 0 | 0 | 0 | 9 | 33-42 | 5 |
| 05:00 | 0 | 0 | 0 | 1 | 0 | 1 | 11 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 40-49 | 16 |
| 06:00 | 0 | 0 | 0 | 0 | 4 | 10 | 23 | 10 | 3 | 0 | 0 | 0 | 0 | 0 | 50 | 36-45 | 33 |
| 07:00 | 0 | 0 | 0 | 0 | 3 | 14 | 25 | 10 | 3 | 2 | 0 | 0 | 0 | 0 | 57 | 36-45 | 39 |
| 08:00 | 0 | 0 | 0 | 0 | 4 | 19 | 35 | 19 | 1 | 1 | 0 | 0 | 0 | 0 | 79 | 37-46 | 55 |
| 09:00 | 0 | 0 | 0 | 2 | 16 | 26 | 47 | 23 | 4 | 0 | 0 | 0 | 0 | 0 | 118 | 36-45 | 73 |
| 10:00 | 1 | 0 | 0 | 2 | 5 | 39 | 49 | 18 | 6 | 1 | 0 | 0 | 0 | 0 | 121 | 36-45 | 88 |
| 11:00 | 0 | 0 | 0 | 3 | 5 | 43 | 48 | 28 | 3 | 3 | 0 | 0 | 0 | 0 | 133 | 36-45 | 91 |
| 12 PM | 0 | 0 | 1 | 0 | 12 | 44 | 53 | 18 | 3 | 0 | 0 | 0 | 0 | 0 | 131 | 36-45 | 97 |
| 13:00 | 0 | 0 | 0 | 2 | 10 | 59 | 41 | 13 | 2 | 0 | 0 | 0 | 0 | 0 | 127 | 36-45 | 100 |
| 14:00 | 0 | 0 | 0 | 1 | 8 | 21 | 34 | 34 | 3 | 1 | 0 | 0 | 0 | 0 | 102 | 41-50 | 68 |
| 15:00 | 0 | 0 | 0 | 0 | 4 | 22 | 47 | 25 | 3 | 2 | 0 | 0 | 0 | 0 | 103 | 39-48 | 72 |
| 16:00 | 0 | 0 | 0 | 1 | 3 | 30 | 51 | 29 | 1 | 1 | 0 | 0 | 0 | 0 | 116 | 36-45 | 81 |
| 17:00 | 0 | 0 | 0 | 2 | 6 | 19 | 57 | 22 | 1 | 0 | 0 | 0 | 0 | 0 | 107 | 38-47 | 79 |
| 18:00 | 0 | 0 | 0 | 1 | 6 | 27 | 39 | 23 | 2 | 2 | 0 | 0 | 0 | 0 | 100 | 36-45 | 66 |
| 19:00 | 0 | 1 | 1 | 2 | 6 | 32 | 35 | 11 | 0 | 0 | 0 | 0 | 0 | 0 | 88 | 36-45 | 67 |
| 20:00 | 0 | 0 | 0 | 0 | 6 | 17 | 23 | 8 | 2 | 0 | 1 | 0 | 0 | 0 | 57 | 36-45 | 40 |
| 21:00 | 0 | 0 | 0 | 1 | 7 | 20 | 30 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 63 | 36-45 | 50 |
| 22:00 | 0 | 0 | 0 | 0 | 9 | 14 | 14 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 41 | 35-44 | 28 |
| 23:00 | 0 | 0 | 0 | 0 | 2 | 7 | 12 | 5 | 1 | 2 | 0 | 0 | 0 | 0 | 29 | 36-45 | 19 |
| Total | 1 | 1 | 2 | 20 | 119 | 475 | 693 | 316 | 47 | 16 | 2 | 0 | 0 | 0 | 1692 |  |  |
| Percent | 0.1\% | 0.1\% | 0.1\% | 1.2\% | 7.0\% | 28.1\% | 41.0\% | 18.7\% | 2.8\% | 0.9\% | 0.1\% | 0.0\% | 0.0\% | 0.0\% |  |  |  |
| AM Peak | 10:00 |  |  | 11:00 | 09:00 | 11:00 | 10:00 | 11:00 | 10:00 | 11:00 | 01:00 |  |  |  | 11:00 |  |  |
| Vol. | 1 |  |  | 3 | 16 | 43 | 49 | 28 | 6 | 3 | 1 |  |  |  | 133 |  |  |
| PM Peak |  | 19:00 | 12:00 | 13:00 | 12:00 | 13:00 | 17:00 | 14:00 | 12:00 | 15:00 | 20:00 |  |  |  | 12:00 |  |  |
| Vol. |  | 1 | 1 | 2 | 12 | 59 | 57 | 34 | 3 | 2 | 1 |  |  |  | 131 |  |  |

63 Sugar Maple Lane
Kensington, Connecticut 06037
(860) 828-1693

Site Code: 2205
Station ID:


# Connecticut Counts LLC <br> 63 Sugar Maple Lane <br> Kensington, Connecticut 06037 <br> (860) 828-1693 

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Preston Avenue South of 1-91 Ramps Meriden, Connecticut

Site Code: 2205 Station ID:

| Southbound |  |  |  |  |  |  |  |  |  |  |  |  |  |  | Latitude: 0' 0.000 Undefined |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start | 0 | 16 | 21 | 26 | 31 | 36 | 41 | 46 | 51 | 56 | 61 | 66 | 71 | 76 |  | Pace | Number |
| Time | 15 | 20 | 25 | 30 | 35 | 40 | 45 | 50 | 55 | 60 | 65 | 70 | 75 | 9999 | Total | Speed | in Pace |
| 6/14/10 | 0 | 0 | 0 | 2 | 1 | 2 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 34-43 | 6 |
| 01:00 | 0 | 0 | 0 | 0 | 1 | 4 | 1 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 7 | 32-41 | 6 |
| 02:00 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 6 | 38-47 | 5 |
| 03:00 | 0 | 0 | 0 | 0 | 0 | 1 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 38-47 | 5 |
| 04:00 | 0 | 0 | 0 | 4 | 6 | 1 | 2 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 15 | 26-35 | 10 |
| 05:00 | 0 | 0 | 2 | 4 | 5 | 12 | 23 | 8 | 1 | 1 | 0 | 0 | 0 | 0 | 56 | 36-45 | 35 |
| 06:00 | 0 | 0 | 1 | 1 | 2 | 36 | 65 | 30 | 3 | 4 | 0 | 0 | 0 | 0 | 142 | 36-45 | 101 |
| 07:00 | 1 | 1 | 0 | 2 | 11 | 68 | 123 | 47 | 6 | 1 | 0 | 0 | 0 | 0 | 260 | 36-45 | 191 |
| 08:00 | 0 | 0 | 0 | 1 | 14 | 62 | 90 | 28 | 4 | 2 | 1 | 0 | 0 | 0 | 202 | 36-45 | 152 |
| 09:00 | 0 | 0 | 0 | 2 | 7 | 28 | 41 | 17 | 3 | 2 | 0 | 0 | 0 | 0 | 100 | 36-45 | 69 |
| 10:00 | 0 | 0 | 0 | 1 | 13 | 20 | 37 | 18 | 3 | 0 | 0 | 0 | 0 | 0 | 92 | 36-45 | 57 |
| 11:00 | 0 | 0 | 1 | 4 | 10 | 26 | 42 | 15 | 2 | 1 | 0 | 0 | 0 | 0 | 101 | 36-45 | 68 |
| 12 PM | 0 | 0 | 3 | 5 | 12 | 36 | 34 | 15 | 0 | 0 | 0 | 0 | 0 | 0 | 105 | 36-45 | 70 |
| 13:00 | 0 | 0 | 1 | 4 | 8 | 29 | 45 | 16 | 2 | 0 | 0 | 0 | 0 | 0 | 105 | 36-45 | 74 |
| 14:00 | 0 | 0 | 3 | 1 | 14 | 32 | 55 | 20 | 2 | 2 | 0 | 0 | 0 | 0 | 129 | 36-45 | 87 |
| 15:00 | 2 | 0 | 0 | 0 | 4 | 38 | 61 | 16 | 1 | 1 | 0 | 0 | 0 | 0 | 123 | 36-45 | 99 |
| 16:00 | 0 | 0 | 1 | 0 | 10 | 46 | 72 | 25 | 5 | 1 | 0 | 0 | 0 | 1 | 161 | 36-45 | 118 |
| 17:00 | 0 | 0 | 1 | 0 | 11 | 57 | 109 | 35 | 4 | 1 | 0 | 0 | 0 | 1 | 219 | 36-45 | 166 |
| 18:00 | 0 | 0 | 0 | 2 | 8 | 28 | 44 | 25 | 4 | 0 | 0 | 0 | 0 | 0 | 111 | 36-45 | 72 |
| 19:00 | 0 | 0 | 1 | 1 | 11 | 24 | 32 | 10 | 5 | 0 | 0 | 0 | 0 | 0 | 84 | 36-45 | 56 |
| 20:00 | 0 | 0 | 0 | 2 | 4 | 21 | 24 | 12 | 1 | 1 | 0 | 0 | 0 | 0 | 65 | 36-45 | 45 |
| 21:00 | 0 | 0 | 0 | 2 | 7 | 8 | 11 | 8 | 0 | 0 | 0 | 1 | 0 | 0 | 37 | 38-47 | 21 |
| 22:00 | 0 | 0 | 0 | 0 | 6 | 13 | 14 | 6 | 1 | 1 | 0 | 0 | 0 | 0 | 41 | 35-44 | 27 |
| 23:00 | 0 | 0 | 1 | 0 | 0 | 4 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 9 | 35-44 | 8 |
| Total | 3 | 1 | 15 | 38 | 165 | 596 | 937 | 357 | 49 | 18 | 1 | 1 | 0 | 2 | 2183 |  |  |
| Percent | 0.1\% | 0.0\% | 0.7\% | 1.7\% | 7.6\% | 27.3\% | 42.9\% | 16.4\% | 2.2\% | 0.8\% | 0.0\% | 0.0\% | 0.0\% | 0.1\% |  |  |  |
| AM Peak | 07:00 | 07:00 | 05:00 | 04:00 | 08:00 | 07:00 | 07:00 | 07:00 | 07:00 | 06:00 | 08:00 |  |  |  | 07:00 |  |  |
| Vol. | 1 | 1 | 2 | 4 | 14 | 68 | 123 | 47 | 6 | 4 | 1 |  |  |  | 260 |  |  |
| PM Peak | 15:00 |  | 12:00 | 12:00 | 14:00 | 17:00 | 17:00 | 17:00 | 16:00 | 14:00 |  | 21:00 |  | 16:00 | 17:00 |  |  |
| Vol. | 2 |  | 3 | 5 | 14 | 57 | 109 | 35 | 5 | 2 |  | 1 |  | 1 | 219 |  |  |



# Connecticut Counts LLC 

Kensington, Connecticut 06037
East Main Street at Preston/Cone Avenue (860) 828-1693
File Name : 9806
Meriden, Connecticut
Site Code : 9806
Start Date : 6/14/2010
Page No : 1


# Connecticut Counts LLC 

Kensington, Connecticut 06037
(860) 828-1693

File Name : 9806
Site Code : 9806
Start Date : 6/14/2010
Page No : 2

|  | Preston Avenue From North |  |  |  |  | East Main Street From East |  |  |  |  | Cone Avenue From South |  |  |  |  | East Main Street From West |  |  |  |  | ne. Toal |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Pcds | App Total | Right | Thru | Left | Peds | App Tout | Right | Thru | Left | Peds | Appr Total | Right | Thru | Left | Peds | App Toual |  |
| Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 07:30 AM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 07:30 AM | 67 | 9 | 8 | 0 | 84 | 13 | 52 | 0 | 0 | 65 | 2 | 15 | 12 | 0 | 29 | 10 | 63 | 32 | 0 | 105 | 283 |
| 07:45 AM | 87 | 9 | 10 | 0 | 106 | 11 | 64 | 1 | 0 | 76 | 0 | 15 | 21 | 0 | 36 | 11 | 38 | 28 | 0 | 77 | 295 |
| 08:00 AM | 64 | 9 | 8 | 0 | 81 | 9 | 47 | 0 | 0 | 56 | 1 | 18 | 6 | 0 | 25 | 5 | 54 | 33 | 0 | 92 | 254 |
| 08:15 AM | 45 | 5 | 3 | 0 | 53 | 10 | 47 | 0 | 0 | 57 | 1 | 14 | 11 | 0 | 26 | 9 | 37 | 22 | 0 | 68 | 204 |
| Total Volume | 263 | 32 | 29 | 0 | 324 | 43 | 210 | 1 | 0 | 254 | 4 | 62 | 50 | 0 | 116 | 35 | 192 | 115 | 0 | 342 | 1036 |
| \%App. Total | 81.2 | 9.9 | 9 | 0 |  | 16.9 | 82.7 | 0.4 | 0 |  | 3.4 | 53.4 | 43.1 | 0 |  | 10.2 | 56.1 | 33.6 | 0 |  |  |
| PHF | . 756 | . 889 | . 725 | . 000 | . 764 | . 827 | . 820 | . 250 | . 000 | . 836 | . 500 | . 861 | . 595 | . 000 | . 806 | . 795 | . 762 | . 871 | . 000 | . 814 | . 878 |



## Connecticut Counts LLC

Kensington, Connecticut 06037
(860) 828-1693

File Name : 9806
Site Code : 9806
Start Date : 6/14/2010
Page No : 3

|  | Preston Avenue From North |  |  |  |  | East Main Street From East |  |  |  |  | Cone Avenue From South |  |  |  |  | East Main Street From West |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Apt Total | Right | Thru | Left | Peds | App Tobal | Right | Thru | Left | Peds | App. Teat | Right | Thru | Left | Peds | App Toul |

Peak Hour Analysis From 07:00 AM to 08:45 AM - Peak 1 of 1
Peak Hour for Each Approach Begins at:

|  | 0730 Am |  |  |  |  | 9730 ^M |  |  |  |  | 07:00 AM |  |  |  |  | 07:1sam |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| +0 mins. | 67 | 9 | 8 | 0 | 84 | 13 | 52 | 0 | 0 | 65 | 0 | 18 | 18 | 0 | 36 | 8 | 40 | 28 | 0 | 76 |
| +15 mins. | 87 | 9 | 10 | 0 | 106 | 11 | 64 | 1 | 0 | 76 | 0 | 10 | 16 | 0 | 26 | 10 | 63 | 32 | 0 | 105 |
| +30 mins. | 64 | 9 | 8 | 0 | 81 | 9 | 47 | 0 | 0 | 56 | 2 | 15 | 12 | 0 | 29 | 11 | 38 | 28 | 0 | 77 |
| +45 mins. | 45 | 5 | 3 | 0 | 53 | 10 | 47 | 0 | 0 | 57 | 0 | 15 | 21 | 0 | 36 | 5 | 54 | 33 | 0 | 92 |
| Total Volume | 263 | 32 | 29 | 0 | 324 | 43 | 210 | 1 | 0 | 254 | 2 | 58 | 67 | 0 | 127 | 34 | 195 | 121 | 0 | 350 |
| \% App. Total | 81.2 | 9.9 | 9 | 0 |  | 16.9 | 82.7 | 0.4 | 0 |  | 1.6 | 45.7 | 52.8 | 0 |  | 9.7 | 55.7 | 34.6 | 0 |  |
| PHF | . 756 | . 889 | . 725 | . 000 | . 764 | . 827 | . 820 | . 250 | . 000 | . 836 | . 250 | . 806 | . 798 | . 000 | . 882 | . 773 | . 774 | . 917 | . 000 | . 833 |



# Connecticut Counts LLC 

Kensington, Connecticut 06037
East Main Street at Preston/Cone Avenue (860) 828-1693
File Name : 9807 Meriden, Connecticut

Site Code : 9807
Start Date : 6/14/2010
Page No : 1

Groups Printed- Unshifted - Bank 1 - Bank 2

| Groups Printed- Unshifted - Bank 1-Bank 2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | Preston Avenue From North |  |  |  |  | East Main Street From East |  |  |  |  | Cone Avenue From South |  |  |  |  | East Main Street From West |  |  |  |  | Tot Total |
| Start Time | Right | Thru | Left | Peds | App Total | Right | Thru | Left | Peds | Apm Toat | Right | Thru | Left | Peds | Apr Tetal | Right | Thru | Left | Peds | App. Total |  |
| 04:00 PM | 16 | 14 | 11 | 0 | 41 | 7 | 44 | 1 | 0 | 52 | 0 | 12 | 6 | 0 | 18 | 22 | 94 | 55 | 0 | 171 | 282 |
| 04:15 PM | 30 | 13 | 15 | 0 | 58 | 4 | 35 | 1 | 0 | 40 | 0 | 14 | 14 | 0 | 28 | 18 | 78 | 43 | 0 | 139 | 265 |
| 04:30 PM | 36 | 27 | 10 | 0 | 73 | 7 | 47 | 1 | 0 | 55 | 0 | 10 | 8 | 0 | 18 | 21 | 86 | 76 | 0 | 183 | 329 |
| 04:45 PM | 22 | 16 | 13 | 0 | 51 | 10 | 69 | 1 | 0 | 80 | 2 | 16 | 13 | 0 | 31 | 34 | 81 | 83 | 0 | 198 | 360 |
| Total | 104 | 70 | 49 | 0 | 223 | 28 | 195 | 4 | 0 | 227 | 2 | 52 | 41 | 0 | 95 | 95 | 339 | 257 | 0 | 691 | 1236 |
| 05:00 PM | 28 | 19 | 15 | 0 | 62 | 15 | 49 | 0 | 0 | 64 | 1 | 12 | 21 | 0 | 34 | 22 | 113 | 108 | 0 | 243 | 403 |
| 05:15 PM | 38 | 33 | 13 | 0 | 84 | 7 | 43 | 0 | 0 | 50 | 3 | 16 | 18 | 0 | 37 | 37 | 84 | 90 | 0 | 211 | 382 |
| 05:30 PM | 32 | 35 | 17 | 0 | 84 | 9 | 64 | 1 | 0 | 74 | 2 | 12 | 18 | 0 | 32 | 43 | 82 | 61 | 0 | 186 | 376 |
| 05:45 PM | 29 | 42 | 15 | 0 | 86 | 7 | 32 | 0 | 0 | 39 | 2 | 14 | 22 | 0 | 38 | 37 | 88 | 57 | 0 | 182 | 345 |
| Total | 127 | 129 | 60 | 0 | 316 | 38 | 188 | 1 | 0 | 227 | 8 | 54 | 79 | 0 | 141 | 139 | 367 | 316 | 0 | 822 | 1506 |
| Grand Total | 231 | 199 | 109 | 0 | 539 | 66 | 383 | 5 | 0 | 454 | 10 | 106 | 120 | 0 | 236 | 234 | 706 | 573 | 0 | 1513 | 2742 |
| Apprch \% | 42.9 | 36.9 | 20.2 | 0 |  | 14.5 | 84.4 | 1.1 | 0 |  | 4.2 | 44.9 | 50.8 | 0 |  | 15.5 | 46.7 | 37.9 | 0 |  |  |
| Total \% | 8.4 | 7.3 | 4 | 0 | 19.7 | 2.4 | 14 | 0.2 | 0 | 16.6 | 0.4 | 3.9 | 4.4 | 0 | 8.6 | 8.5 | 25.7 | 20.9 | 0 | 55.2 |  |
| Unshifted | 221 | 199 | 109 | 0 | 529 | 66 | 376 | 5 | 0 | 447 | 9 | 106 | 119 | 0 | 234 | 233 | 696 | 557 | 0 | 1486 | 2696 |
| \% Unshifted | 95.7 | 100 | 100 | 0 | 98.1 | 100 | 98.2 | 100 | 0 | 98.5 | 90 | 100 | 99.2 | 0 | 99.2 | 99.6 | 98.6 | 97.2 | 0 | 98.2 | 98.3 |
| Bank 1 | 10 | 0 | 0 | 0 | 10 | 0 | 7 | 0 | 0 | 7 | 1 | 0 | 0 | 0 | 1 | 1 | 9 | 16 | 0 | 26 | 44 |
| \% Bank 1 | 4.3 | 0 | 0 | 0 | 1.9 | 0 | 1.8 | 0 | 0 | 1.5 | 10 | 0 | 0 | 0 | 0.4 | 0.4 | 1.3 | 2.8 | 0 | 1.7 | 1.6 |
| Bank 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 | 1 | 0 | 1 | 0 | 0 | 1 | 2 |
| \% Bank 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0.8 | 0 | 0.4 | 0 | 0.1 | 0 | 0 | 0.1 | 0.1 |

File Name : 9807
Site Code : 9807
Start Date : 6/14/2010
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|  | Preston Avenue From North |  |  |  |  | East Main Street From East |  |  |  |  | Cone Avenue From South |  |  |  |  | East Main Street From West |  |  |  |  | In. Toual |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Start Time | Right | Thru | Left | Peds | Apn Teal | Right | Thru | Left | Peds | App Toat | Right | Thru | Left | Peds | Apm. Total | Right | Thru | Left | Peds | App Toud |  |
| Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| Peak Hour for Entire Intersection Begins at 04:45 PM |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 04:45 PM | 22 | 16 | 13 | 0 | 51 | 10 | 69 | 1 | 0 | 80 | 2. | 16 | 13 | 0 | 31 | 34 | 81 | 83 | 0 | 198 | 360 |
| 05:00 PM | 28 | 19 | 15 | 0 | 62 | 15 | 49 | 0 | 0 | 64 | 1 | 12 | 21 | 0 | 34 | 22 | 113 | 108 | 0 | 243 | 403 |
| 05:15 PM | 38 | 33 | 13 | 0 | 84 | 7 | 43 | 0 | 0 | 50 | 3 | 16 | 18 | 0 | 37 | 37 | 84 | 90 | 0 | 211 | 382 |
| 05:30 PM | 32 | 35 | 17 | 0 | 84 | 9 | 64 | 1 | 0 | 74 | 2 | 12 | 18 | 0 | 32 | 43 | 82 | 61 | 0 | 186 | 376 |
| Total Volume | 120 | 103 | 58 | 0 | 281 | 41 | 225 | 2 | 0 | 268 | 8 | 56 | 70 | 0 | 134 | 136 | 360 | 342 | 0 | 838 | 1521 |
| \%App. Total | 42.7 | 36.7 | 20.6 | 0 |  | 15.3 | 84 | 0.7 | 0 |  | 6 | 41.8 | 52.2 | 0 |  | 16.2 | 43 | 40.8 | 0 |  |  |
| PHF | . 789 | . 736 | . 853 | . 000 | . 836 | . 683 | . 815 | . 500 | . 000 | . 838 | . 667 | . 875 | . 833 | . 000 | . 905 | . 791 | . 796 | . 792 | . 000 | . 862 | . 944 |



## Connecticut Counts LLC

Kensington, Connecticut 06037
(860) 828-1693

File Name : 9807
Site Code : 9807
Start Date : 6/14/2010
Page No : 3


Peak Hour Analysis From 04:00 PM to 05:45 PM - Peak 1 of 1
Peak Hour for Each Approach Begins at:

| +0 mins. | 05sao PM |  |  |  |  | ouss PM |  |  |  |  | (15sua PM |  |  |  |  | O4: 5 PM |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | 28 | 19 | 15 | 0 | 62 | 10 | 69 | 1 | 0 | 80 | 1 | 12 | 21 | 0 | 34 | 34 | 81 | 83 | 0 | 198 |
| +15 mins. | 38 | 33 | 13 | 0 | 84 | 15 | 49 | 0 | 0 | 64 | 3 | 16 | 18 | 0 | 37 | 22 | 113 | 108 | 0 | 243 |
| +30 mins. | 32 | 35 | 17 | 0 | 84 | 7 | 43 | 0 | 0 | 50 | 2 | 12 | 18 | 0 | 32 | 37 | 84 | 90 | 0 | 211 |
| +45 mins. | 29 | 42 | 15 | 0 | 86 | 9 | 64 | 1 | 0 | 74 | 2 | 14 | 22 | 0 | 38 | 43 | 82 | 61 | 0 | 186 |
| Total Volume | 127 | 129 | 60 | 0 | 316 | 41 | 225 | 2 | 0 | 268 | 8 | 54 | 79 | 0 | 141 | 136 | 360 | 342 | 0 | 838 |
| \% App. Total | 40.2 | 40.8 | 19 | 0 |  | 15.3, | 84 | 0.7 | 0 |  | 5.7 | 38.3 | 56 | 0 |  | 16.2 | 43 | 40.8 | 0 |  |
| PHF | . 836 | . 768 | . 882 | . 000 | . 919 | . 683 | . 815 | . 500 | . 000 | . 838 | . 667 | . 844 | . 898 | . 000 | . 928 | . 791 | . 796 | . 792 | . 000 | . 862 |



## Appendix B

2010 Weekday Capacity Analysis - Preston Avenue at East Main Street

|  | - | $\rightarrow$ | - | 5 | 4 | 央 | 4 | $\dagger$ | \% | $\pm$ | $4$ | $\frac{1}{7}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL2 | WBT | WBR | NBL | NBT | NBR | SBL2 | SBL | SBT |
| Lane Configurations | ${ }^{7}$ | $\hat{\dagger}$ |  |  | * |  |  | * |  |  |  | ¢ |
| Volume (vph) | 115 | 192 | 35 | 1 | 210 | 43 | 5 | 5 | 5 | 29 | 32 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 130 |  | 0 |  |  | 0 | 0 |  | 0 |  | 0 |  |
| Storage Lanes | 1 |  | 0 |  |  | 0 | 0 |  | 0 |  | 0 |  |
| Taper Length ( ft ) | 25 |  | 25 |  |  | 25 | 25 |  | 25 |  | 25 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.977 |  |  | 0.977 |  |  | 0.955 |  |  |  | 0.890 |
| Flt Protected | 0.950 |  |  |  |  |  |  | 0.984 |  |  |  | 0.991 |
| Satd. Flow (prot) | 1770 | 1820 | 0 | 0 | 1820 | 0 | 0 | 1750 | 0 | 0 | 0 | 1643 |
| Flt Permitted | 0.375 |  |  |  | 0.999 |  |  | 0.891 |  |  |  | 0.931 |
| Satd. Flow (perm) | 699 | 1820 | 0 | 0 | 1818 | 0 | 0 | 1585 | 0 | 0 | 0 | 1543 |
| Right Turn on Red |  |  |  |  |  | Yes |  |  |  |  |  |  |
| Satd. Flow (RTOR) |  |  |  |  | 15 |  |  |  |  |  |  | 331 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  |  | 30 |
| Link Distance (ft) |  | 402 |  |  | 913 |  |  | 376 |  |  |  | 1042 |
| Travel Time (s) |  | 9.1 |  |  | 20.8 |  |  | 8.5 |  |  |  | 23.7 |
| Peak Hour Factor | 0.81 | 0.81 | 0.81 | 0.84 | 0.84 | 0.84 | 0.92 | 0.92 | 0.92 | 0.76 | 0.76 | 0.76 |
| Adj. Flow (vph) | 142 | 237 | 43 | 1 | 250 | 51 | 5 | 5 | 5 | 38 | 42 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 142 | 280 | 0 | 0 | 302 | 0 | 0 | 15 | 0 | 0 | 0 | 426 |
| Turn Type | pm+pt |  |  | Perm |  |  | Perm |  |  | Perm | Perm |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 2 |  |  |  | 6 |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 | 6 | 6 |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 4.0 | 15.0 |  | 15.0 | 15.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 6.0 | 21.0 |  | 21.0 | 21.0 |  | 14.0 | 14.0 |  | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 6.0 | 27.0 | 0.0 | 21.0 | 21.0 | 0.0 | 24.0 | 24.0 | 0.0 | 24.0 | 24.0 | 24.0 |
| Total Split (\%) | 9.2\% | 41.5\% | 0.0\% | 32.3\% | 32.3\% | 0.0\% | 36.9\% | 36.9\% | 0.0\% | 36.9\% | 36.9\% | 36.9\% |
| Maximum Green (s) | 4.0 | 21.0 |  | 15.0 | 15.0 |  | 18.0 | 18.0 |  | 18.0 | 18.0 | 18.0 |
| Yellow Time (s) | 2.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 2.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | Max | Max |  | Max | Max | Max |
| v/c Ratio | 0.43 | 0.50 |  |  | 0.69 |  |  | 0.03 |  |  |  | 0.63 |
| Control Delay | 18.3 | 21.4 |  |  | 31.4 |  |  | 17.6 |  |  |  | 10.1 |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  |  | 0.0 |
| Total Delay | 18.3 | 21.4 |  |  | 31.4 |  |  | 17.6 |  |  |  | 10.1 |
| Queue Length 50th (ft) | 36 | 87 |  |  | 104 |  |  | 4 |  |  |  | 29 |
| Queue Length 95th ( ft ) | 63 | 133 |  |  | \#168 |  |  | 17 |  |  |  | 60 |
| Internal Link Dist (ft) |  | 322 |  |  | 833 |  |  | 296 |  |  |  | 962 |
| Turn Bay Length ( ft ) | 130 |  |  |  |  |  |  |  |  | . |  |  |
| Base Capacity (vph) | 328 | 600 |  |  | 439 |  |  | 448 |  |  |  | 674 |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |


| Lane Group | SBR | NWL | NWR | NWR2 |
| :---: | :---: | :---: | :---: | :---: |
| Landsonfigurations |  | \% |  |  |
| Volume (vph) | 263 | 50 | 62 | 4 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 |
| Storage Length (tt) | 0 | 0 | 0 |  |
| Storage Lanes | 0 | 1 | 0 |  |
| Taper Length (ft) | 25 | 25 | 25 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.923 |  |  |
| Flt Protected |  | 0.979 |  |  |
| Satd. Flow (prot) | 0 | 1683 | 0 | 0 |
| Flt Permitted |  | 0.979 |  |  |
| Satd. Flow (perm) | 0 | 1683 | 0 | 0 |
| Right Turn on Red | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 2 |  |  |
| Link Speed (mph) |  | 30 |  |  |
| Link Distance ( ft ) |  | 264 |  |  |
| Travel Time (s) |  | 6.0 |  |  |
| Peak Hour Factor | 0.76 | 0.81 | 0.81 | 0.81 |
| Adj. Flow (vph) | 346 | 62 | 77 | 5 |
| Shared Lane Traffic (\%) |  |  |  |  |
| Lane Group Flow (vph) | 0 | 144 | 0 | 0 |
| Turn Type |  |  |  |  |
| Protected Phases |  | 5 |  |  |
| Permitted Phases |  | 5 |  |  |
| Detector Phase |  | 5 |  |  |
| Switch Phase |  |  |  |  |
| Minimum Initial (s) |  | 8.0 |  |  |
| Minimum Split (s) |  | 14.0 |  |  |
| Total Split (s) | 0.0 | 14.0 | 0.0 | 0.0 |
| Total Split (\%) | 0.0\% | 21.5\% | 0.0\% | 0.0\% |
| Maximum Green (s) |  | 8.0 |  |  |
| Yellow Time (s) |  | 4.0 |  |  |
| All-Red Time (s) |  | 2.0 |  |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.0 | 6.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |
| Vehicle Extension (s) |  | 3.0 |  |  |
| Recall Mode |  | Max |  |  |
| $\mathrm{v} / \mathrm{C}$ Ratio |  | 0.68 |  |  |
| Control Delay |  | 45.3 |  |  |
| Queue Delay |  | 0.0 |  |  |
| Total Delay |  | 45.3 |  |  |
| Queue Length 50th (ft) |  | 55 |  |  |
| Queue Length 95th (ft) |  | \#112 |  |  |
| Internal Link Dist (ft) |  | 184 |  |  |
| Turn Bay Length (ft) |  |  |  |  |
| Base Capacity (vph) |  | 213 |  |  |
| Starvation Cap Reductn |  | 0 |  |  |


|  | $\rangle$ | $\rightarrow$ | 7 | 5 | - | 4 | 4 | $\uparrow$ | $>$ | $\checkmark$ | W | ¢ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL2 | WBT | WBR | NBL | NBT | NBR | SBL2 | SBL | SBT |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |
| Reduced v/c Ratio | 0.43 | 0.47 |  |  | 0.69 |  |  | 0.03 |  |  |  | 0.63 |

## Intersection Summary

## Area Type:

Other

Cycle Length: 65
Actuated Cycle Length: 63.8
Natural Cycle: 55
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: East Main Street \& Preston Avenue


1: East Main Street \& Preston Avenue

|  |  |  |  |  |
| :--- | ---: | ---: | ---: | ---: |
| Lane Group | SBR | NWL | NWR | NWR2 |
| Spillback Cap Reductn | 0 |  |  |  |
| Storage Cap Reductn | 0 |  |  |  |
| Reduced v/c Ratio | 0.68 |  |  |  |
| Intersection Summary |  |  |  |  |


c Critical Lane Group

|  | $\downarrow$ | 4 | 4 | $\stackrel{ }{ }+$ |
| :---: | :---: | :---: | :---: | :---: |
| Movement | SBR | NWL | NWR | NWR2 |
| Lan\$¢onfigurations |  | ${ }^{4}$ |  |  |
| Volume (vph) | 263 | 50 | 62 | 4 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.0 |  |  |
| Lane Util. Factor |  | 1.00 |  |  |
| Fit |  | 0.92 |  |  |
| Flt Protected |  | 0.98 |  |  |
| Satd. Flow (prot) |  | 1683 |  |  |
| Flt Permitted |  | 0.98 |  |  |
| Satd. Flow (perm) |  | 1683 |  |  |
| Peak-hour factor, PHF | 0.76 | 0.81 | 0.81 | 0.81 |
| Adj. Flow (vph) | 346 | 62 | 77 | 5 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 142 | 0 | 0 |
| Turn Type |  |  |  |  |
| Protected Phases |  | 5 |  |  |
| Permitted Phases |  | 5 |  |  |
| Actuated Green, G (s) |  | 8.0 |  |  |
| Effective Green, $\mathrm{g}(\mathrm{s})$ |  | 8.0 |  |  |
| Actuated g/C Ratio |  | 0.12 |  |  |
| Clearance Time (s) |  | 6.0 |  |  |
| Vehicle Extension (s) |  | 3.0 |  |  |
| Lane Grp Cap (vph) |  | 210 |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Prot |  | c0.08 |  |  |
| v/s Ratio Perm |  |  |  |  |
| v/c Ratio |  | 0.68 |  |  |
| Uniform Delay, d1 |  | 26.8 |  |  |
| Progression Factor |  | 1.00 |  |  |
| Incremental Delay, d2 |  | 16.2 |  |  |
| Delay (s) |  | 43.0 |  |  |
| Level of Service |  | D |  |  |
| Approach Delay (s) |  | 43.0 |  |  |
| Approach LOS |  | D |  |  |
| Intersection Summary |  |  |  |  |


|  | 务 | $\rightarrow$ | T | 系 | 4 | 4 | 4 | $\dagger$ | $p$ | * | $4$ | $\frac{1}{7}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL2 | WBT | WBR | NBL | NBT | NBR | SBL2 | SBL | SBT |
| Lane Configurations | ${ }^{7}$ | $\hat{\square}$ |  |  | 4 |  |  | * |  |  |  | ¢ |
| Volume (vph) | 342 | 360 | 136 | 2 | 225 | 41 | 5 | 5 | 5 | 58 | 103 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length ( ft ) | 130 |  | 0 |  |  | 0 | 0 |  | 0 |  | 0 |  |
| Storage Lanes | 1 |  | 0 |  |  | 0 | 0 |  | 0 |  | 0 |  |
| Taper Length (ft) | 25 |  | 25 |  |  | 25 | 25 |  | 25 |  | 25 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.959 |  |  | 0.979 |  |  | 0.955 |  |  |  | 0.942 |
| Flt Protected | 0.950 |  |  |  |  |  |  | 0.984 |  |  |  | 0.972 |
| Satd. Flow (prot) | 1770 | 1786 | 0 | 0 | 1824 | 0 | 0 | 1750 | 0 | 0 | 0 | 1706 |
| Flt Permitted | 0.346 |  |  |  | 0.995 |  |  | 0.882 |  |  |  | 0.814 |
| Satd. Flow (perm) | 645 | 1786 | 0 | 0 | 1815 | 0 | 0 | 1569 | 0 | 0 | 0 | 1428 |
| Right Turn on Red |  |  |  |  |  | Yes |  |  |  |  |  |  |
| Satd. Flow (RTOR) |  |  |  |  | 13 |  |  |  |  |  |  | 52 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  |  | 30 |
| Link Distance (ft) |  | 402 |  |  | 913 |  |  | 376 |  |  |  | 1042 |
| Travel Time (s) |  | 9.1 |  |  | 20.8 |  |  | 8.5 |  |  |  | 23.7 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.84 | 0.84 | 0.84 | 0.92 | 0.92 | 0.92 | 0.84 | 0.84 | 0.84 |
| Adj. Flow (vph) | 398 | 419 | 158 | 2 | 268 | 49 | 5 | 5 | 5 | 69 | 123 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 398 | 577 | 0 | 0 | 319 | 0 | 0 | 15 | 0 | 0 | 0 | 335 |
| Turn Type | pm+pt |  |  | Perm |  |  | Perm |  |  | Perm | Perm |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 2 |  |  |  | 6 |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 | 6 | 6 |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 4.0 | 15.0 |  | 15.0 | 15.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 6.0 | 21.0 |  | 21.0 | 21.0 |  | 14.0 | 14.0 |  | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 11.0 | 32.0 | 0.0 | 21.0 | 21.0 | 0.0 | 19.0 | 19.0 | 0.0 | 19.0 | 19.0 | 19.0 |
| Total Split (\%) | 16.9\% | 49.2\% | 0.0\% | 32.3\% | 32.3\% | 0.0\% | 29.2\% | 29.2\% | 0.0\% | 29.2\% | 29.2\% | 29.2\% |
| Maximum Green (s) | 9.0 | 26.0 |  | 15.0 | 15.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 | 13.0 |
| Yellow Time (s) | 2.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 2.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | Max | Max |  | Max | Max | Max |
| v/c Ratio | 0.88 | 0.81 |  |  | 0.74 |  |  | 0.05 |  |  |  | 1.02 |
| Control Delay | 37.3 | 28.5 |  |  | 35.1 |  |  | 21.6 |  |  |  | 82.6 |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  |  | 0.0 |
| Total Delay | 37.3 | 28.5 |  |  | 35.1 |  |  | 21.6 |  |  |  | 82.6 |
| Queue Length 50th (ft) | 104 | 196 |  |  | 113 |  |  | 5 |  |  |  | $\sim 120$ |
| Queue Length 95th (ft) | \#215 | \#332 |  |  | \#198 |  |  | 19 |  |  |  | \#245 |
| Internal Link Dist (ft) |  | 322 |  |  | 833 |  |  | 296 |  |  |  | 962 |
| Turn Bay Length (ft) | 130 |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 453 | 714 |  |  | 429 |  |  | 314 |  |  |  | 327 |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  |  |



|  | $\rangle$ | $\rightarrow$ | - | - | $\leftarrow$ | 4 | 4 | 4 | $p$ | * | $\cdots$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL2 | WBT | WBR | NBL | NBT | NBR | SBL2 | SBL | SBT |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |
| Reduced v/c Ratio | 0.88 | 0.81 |  |  | 0.74 |  |  | 0.05 |  |  |  | 1.02 |

## Intersection Summary

```
Area Type:
Other
```

Cycle Length: 65
Actuated Cycle Length: 65
Natural Cycle: 70
Control Type: Actuated-Uncoordinated
~ Volume exceeds capacity, queue is theoretically infinite. Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: East Main Street \& Preston Avenue



c Critical Lane Group

|  | $\downarrow$ | 4 | 4 | $\stackrel{+}{ }$ |
| :---: | :---: | :---: | :---: | :---: |
| Movement | SBR | NWL | NWR | NWR2 |
| Lan§§onfigurations |  | \% |  |  |
| Volume (vph) | 120 | 70 | 56 | 8 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.0 |  |  |
| Lane Utill. Factor |  | 1.00 |  |  |
| Fit |  | 0.94 |  |  |
| Flt Protected |  | 0.97 |  |  |
| Satd. Flow (prot) |  | 1698 |  |  |
| Flt Permitted |  | 0.97 |  |  |
| Satd. Flow (perm) |  | 1698 |  |  |
| Peak-hour factor, PHF | 0.84 | 0.91 | 0.91 | 0.91 |
| Adj. Flow (vph) | 143 | 77 | 62 | 9 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 144 | 0 | 0 |
| Turn Type |  |  |  |  |
| Protected Phases |  | 5 |  |  |
| Permitted Phases |  | 5 |  |  |
| Actuated Green, G (s) |  | 8.0 |  |  |
| Effective Green, g (s) |  | 8.0 |  |  |
| Actuated g/C Ratio |  | 0.12 |  |  |
| Clearance Time (s) |  | 6.0 |  |  |
| Vehicle Extension (s) |  | 3.0 |  |  |
| Lane Grp Cap (vph) |  | 209 |  |  |
| v/s Ratio Prot |  | c0.09 |  |  |
| $\mathrm{v} / \mathrm{s}$ Ratio Perm |  |  |  |  |
| $\mathrm{v} / \mathrm{c}$ Ratio |  | 0.69 |  |  |
| Uniform Delay, d1 |  | 27.3 |  |  |
| Progression Factor |  | 1.00 |  |  |
| Incremental Delay, d2 |  | 17.2 |  |  |
| Delay (s) |  | 44.5 |  |  |
| Level of Service |  | D |  |  |
| Approach Delay (s) |  | 44.5 |  |  |
| Approach LOS |  | D |  |  |
| Intersection Summary |  |  |  |  |

## Appendix C

2030 Weekday Capacity Analysis - Preston Avenue at East Main Street

|  | 4 | $\rightarrow$ | 7 | - | $\leftarrow$ | 4 | 4 | 4 | $p$ | $\pm$ | 4 | $\frac{1}{*}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL2 | WBT | WBR | NBL | NBT | NBR | SBL2 | SBL | SBT |
| Lane Configurations | \% | F |  |  | $\uparrow$ |  |  | ¢ |  |  |  | 4 |
| Volume (vph) | 140 | 234 | 43 | 1 | 256 | 52 | 6 | 6 | 6 | 35 | 39 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length ( ft ) | 130 |  | 0 |  |  | 0 | 0 |  | 0 |  | 0 |  |
| Storage Lanes | 1 |  | 0 |  |  | 0 | 0 |  | 0 |  | 0 |  |
| Taper Length (tt) | 25 |  | 25 |  |  | 25 | 25 |  | 25 |  | 25 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.977 |  |  | 0.977 |  |  | 0.955 |  |  |  | 0.890 |
| Flt Protected | 0.950 |  |  |  |  |  |  | 0.984 |  |  |  | 0.991 |
| Satd. Flow (prot) | 1770 | 1820 | 0 | 0 | 1820 | 0 | 0 | 1750 | 0 | 0 | 0 | 1643 |
| Flt Permitted | 0.283 |  |  |  | 0.999 |  |  | 0.840 |  |  |  | 0.929 |
| Satd. Flow (perm) | 527 | 1820 | 0 | 0 | 1818 | 0 | 0 | 1494 | 0 | 0 | 0 | 1540 |
| Right Turn on Red |  |  |  |  |  | Yes |  |  |  |  |  |  |
| Satd. Flow (RTOR) |  |  |  |  | 15 |  |  |  |  |  |  | 333 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  |  | 30 |
| Link Distance ( ft ) |  | 402 |  |  | 913 |  |  | 376 |  |  |  | 1042 |
| Travel Time (s) |  | 9.1 |  |  | 20.8 |  |  | 8.5 |  |  |  | 23.7 |
| Peak Hour Factor | 0.81 | 0.81 | 0.81 | 0.84 | 0.84 | 0.84 | 0.92 | 0.92 | 0.92 | 0.76 | 0.76 | 0.76 |
| Adj. Flow (vph) | 173 | 289 | 53 | 1 | 305 | 62 | 7 | 7 | 7 | 46 | 51 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 173 | 342 | 0 | 0 | 368 | 0 | 0 | 21 | 0 | 0 | 0 | 519 |
| Turn Type | pm+pt |  |  | Perm |  |  | Perm |  |  | Perm | Perm |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 2 |  |  |  | 6 |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 | 6 | 6 |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 4.0 | 15.0 |  | 15.0 | 15.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 6.0 | 21.0 |  | 21.0 | 21.0 |  | 14.0 | 14.0 |  | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 6.0 | 27.0 | 0.0 | 21.0 | 21.0 | 0.0 | 24.0 | 24.0 | 0.0 | 24.0 | 24.0 | 24.0 |
| Total Split (\%) | 9.2\% | 41.5\% | 0.0\% | 32.3\% | 32.3\% | 0.0\% | 36.9\% | 36.9\% | 0.0\% | 36.9\% | 36.9\% | 36.9\% |
| Maximum Green (s) | 4.0 | 21.0 |  | 15.0 | 15.0 |  | 18.0 | 18.0 |  | 18.0 | 18.0 | 18.0 |
| Yellow Time (s) | 2.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 2.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | Max | Max |  | Max | Max | Max |
| v/c Ratio | 0.62 | 0.58 |  |  | 0.85 |  |  | 0.05 |  |  |  | 0.78 |
| Control Delay | 25.9 | 23.1 |  |  | 44.5 |  |  | 17.8 |  |  |  | 17.8 |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  |  | 0.0 |
| Total Delay | 25.9 | 23.1 |  |  | 44.5 |  |  | 17.8 |  |  |  | 17.8 |
| Queue Length 50th (tt) | 45 | 111 |  |  | 134 |  |  | 6 |  |  |  | 60 |
| Queue Length 95th (ft) | 76 | 162 |  |  | \#244 |  |  | 21 |  |  |  | 105 |
| Internal Link Dist (ft) |  | 322 |  |  | 833 |  |  | 296 |  |  |  | 962 |
| Turn Bay Length (tt) | 130 |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 279 | 588 |  |  | 431 |  |  | 414 |  |  |  | 667 |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |



|  | $\Rightarrow$ | $\rightarrow$ | T | 系 | - | 4 | 4 | $\uparrow$ | $>$ | $\checkmark$ | W | ¢ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL2 | WBT | WBR | NBL | NBT | NBR | SBL2 | SBL | SBT |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |
| Reduced v/c Ratio | 0.62 | 0.58 |  |  | 0.85 |  |  | 0.05 |  |  |  | 0.78 |

Intersection Summary
Area Type: Other
Cycle Length: 65
Actuated Cycle Length: 65
Natural Cycle: 60
Control Type: Actuated-Uncoordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: East Main Street \& Preston Avenue


|  | $\downarrow$ | 4 |  | $\stackrel{+}{ }$ |
| :---: | :---: | :---: | :---: | :---: |
| Lane Group | SBR | NWL | NWR | NWR2 |
| Spillback Cap Reductn |  | 0 |  |  |
| Storage Cap Reductn |  | 0 |  |  |
| Reduced v/c Ratio |  | 0.84 |  |  |
| Intersection Summary |  |  |  |  |


c Critical Lane Group

| Movement | SBR | NWL | NWR | NWR2 |
| :---: | :---: | :---: | :---: | :---: |
| Land¢0nfigurations |  | \% |  |  |
| Volume (vph) | 321 | 61 | 76 | 5 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.0 |  |  |
| Lane Util. Factor |  | 1.00 |  |  |
| Frt |  | 0.92 |  |  |
| Flt Protected |  | 0.98 |  |  |
| Satd. Flow (prot) |  | 1683 |  |  |
| Flt Permitted |  | 0.98 |  |  |
| Satd. Flow (perm) |  | 1683 |  |  |
| Peak-hour factor, PHF | 0.76 | 0.81 | 0.81 | 0.81 |
| Adj. Flow (vph) | 422 | 75 | 94 | 6 |
| RTOR Reduction (vph) | 0 | 2 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 173 | 0 | 0 |

Turn Type
Protected Phases 5

Permitted Phases 5
Actuated Green, G (s) 8.0
Effective Green, g (s) 8.0
Actuated g/C Ratio 0.12
Clearance Time (s) 6.0
Vehicle Extension (s) 3.0
Lane Grp Cap (vph) 207
$\mathrm{v} / \mathrm{s}$ Ratio Prot $\quad \mathrm{c} 0.10$
v/s Ratio Perm
$\mathrm{v} / \mathrm{c}$ Ratio 0.84

Uniform Delay, d1 27.9
Progression Factor $\quad 1.00$
Incremental Delay, d2 31.3
Delay (s) 59.2
Level of Service E
Approach Delay (s) 59.2
Approach LOS
E
Intersection Summary

| Lane Group | EBL | EBT | EBR | WBL2 | WBT | WBR | NBL | NBT | NBR | SBL2 | SBL | SBT |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Configurations | \% | $\uparrow$ |  |  | $\uparrow$ |  | - | ¢ |  |  |  | ( |
| Volume (vph) | 417 | 439 | 166 | 2 | 275 | 50 | 6 | 6 | 6 | 71 | 126 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length ( ft ) | 130 |  | 0 |  |  | 0 | 0 |  | 0 |  | 0 |  |
| Storage Lanes | 1 |  | 0 |  |  | 0 | 0 |  | 0 |  | 0 |  |
| Taper Length ( ft ) | 25 |  | 25 |  |  | 25 | 25 |  | 25 |  | 25 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.959 |  |  | 0.979 |  |  | 0.955 |  |  |  | 0.943 |
| Fit Protected | 0.950 |  |  |  |  |  |  | 0.984 |  |  |  | 0.972 |
| Satd. Flow (prot) | 1770 | 1786 | 0 | 0 | 1824 | 0 | 0 | 1750 | 0 | 0 | 0 | 1707 |
| Flt Permitted | 0.259 |  |  |  | 0.962 |  |  | 0.870 |  |  |  | 0.811 |
| Satd. Flow (perm) | 482 | 1786 | 0 | 0 | 1754 | 0 | 0 | 1548 | 0 | 0 | 0 | 1425 |
| Right Turn on Red |  |  |  |  |  | Yes |  |  |  |  |  |  |
| Satd. Flow (RTOR) |  |  |  |  | 13 |  |  |  |  |  |  | 51 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  |  | 30 |
| Link Distance (ft) |  | 402 |  |  | 913 |  |  | 376 |  |  |  | 1042 |
| Travel Time (s) |  | 9.1 |  |  | 20.8 |  |  | 8.5 |  |  |  | 23.7 |
| Peak Hour Factor | 0.86 | 0.86 | 0.86 | 0.84 | 0.84 | 0.84 | 0.92 | 0.92 | 0.92 | 0.84 | 0.84 | 0.84 |
| Adj. Flow (vph) | 485 | 510 | 193 | 2 | 327 | 60 | 7 | 7 | 7 | 85 | 150 | 0 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 485 | 703 | 0 | 0 | 389 | 0 | 0 | 21 | 0 | 0 | 0 | 409 |
| Turn Type | pm+pt |  |  | Perm |  |  | Perm |  |  | Perm | Perm |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 2 |  |  |  | 6 |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 | 6 | 6 |
| Detector Phase | 7 | 4 |  | 8 | 8 |  | 2 | 2 |  | 6 | 6 | 6 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) | 4.0 | 15.0 |  | 15.0 | 15.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 | 8.0 |
| Minimum Split (s) | 6.0 | 21.0 |  | 21.0 | 21.0 |  | 14.0 | 14.0 |  | 14.0 | 14.0 | 14.0 |
| Total Split (s) | 11.0 | 32.0 | 0.0 | 21.0 | 21.0 | 0.0 | 19.0 | 19.0 | 0.0 | 19.0 | 19.0 | 19.0 |
| Total Split (\%) | 16.9\% | 49.2\% | 0.0\% | 32.3\% | 32.3\% | 0.0\% | 29.2\% | 29.2\% | 0.0\% | 29.2\% | 29.2\% | 29.2\% |
| Maximum Green (s) | 9.0 | 26.0 |  | 15.0 | 15.0 |  | 13.0 | 13.0 |  | 13.0 | 13.0 | 13.0 |
| Yellow Time (s) | 2.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 |  | 4.0 | 4.0 | 4.0 |
| All-Red Time (s) | 0.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 2.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 4.0 | 6.0 | 6.0 | 6.0 |
| Lead/Lag | Lead |  |  | Lag | Lag |  |  |  |  |  |  |  |
| Lead-Lag Optimize? | Yes |  |  | Yes | Yes |  |  |  |  |  |  |  |
| Vehicle Extension (s) | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode | None | None |  | None | None |  | Max | Max |  | Max | Max | Max |
| v/c Ratio | 1.21 | 0.98 |  |  | 0.94 |  |  | 0.07 |  |  |  | 1.25 |
| Control Delay | 134.7 | 52.6 |  |  | 58.2 |  |  | 21.9 |  |  |  | 162.2 |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  |  | 0.0 |
| Total Delay | 134.7 | 52.6 |  |  | 58.2 |  |  | 21.9 |  |  |  | 162.2 |
| Queue Length 50th ( ft ) | ~173 | 266 |  |  | 147 |  |  | 7 |  |  |  | ~193 |
| Queue Length 95th ( ft ) | \#317 | \#447 |  |  | \#271 |  |  | 23 |  |  |  | \#318 |
| Internal Link Dist ( ft ) |  | 322 |  |  | 833 |  |  | 296 |  |  |  | 962 |
| Turn Bay Length ( ft ) | 130 |  |  |  |  |  |  |  |  |  |  |  |
| Base Capacity (vph) | 401 | 714 |  |  | 415 |  |  | 310 |  |  |  | 326 |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |


| Lane Group | SBR | NWL | NWR | NWR2 |
| :---: | :---: | :---: | :---: | :---: |
| Lan*Sonfigurations |  | ${ }^{1}$ |  |  |
| Volume (vph) | 146 | 85 | 68 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 |
| Storage Length ( ft ) | 0 | 0 | 0 |  |
| Storage Lanes | 0 | 1 | 0 |  |
| Taper Length (ft) | 25 | 25 | 25 |  |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.935 |  |  |
| Flt Protected |  | 0.975 |  |  |
| Satd. Flow (prot) | 0 | 1698 | 0 | 0 |
| Flt Permitted |  | 0.975 |  |  |
| Satd. Flow (perm) | 0 | 1698 | 0 | 0 |
| Right Turn on Red | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | , |  |  |
| Link Speed (mph) |  | 30 |  |  |
| Link Distance (ft) |  | 264 |  |  |
| Travel Time (s) |  | 6.0 |  |  |
| Peak Hour Factor | 0.84 | 0.91 | 0.91 | 0.91 |
| Adj. Flow (vph) | 174 | 93 | 75 | 11 |
| Shared Lane Traffic (\%) |  |  |  |  |
| Lane Group Flow (vph) | 0 | 179 | 0 | 0 |
| Turn Type |  |  |  |  |
| Protected Phases |  | 5 |  |  |
| Permitted Phases |  | 5 |  |  |
| Detector Phase |  | 5 |  |  |
| Switch Phase |  |  |  |  |
| Minimum Initial (s) |  | 8.0 |  |  |
| Minimum Split (s) |  | 14.0 |  |  |
| Total Split (s) | 0.0 | 14.0 | 0.0 | 0.0 |
| Total Split (\%) | 0.0\% | 21.5\% | 0.0\% | 0.0\% |
| Maximum Green (s) |  | 8.0 |  |  |
| Yellow Time (s) |  | 4.0 |  |  |
| All-Red Time (s) |  | 2.0 |  |  |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 4.0 | 6.0 | 4.0 | 4.0 |
| Lead/Lag |  |  |  |  |
| Lead-Lag Optimize? |  |  |  |  |
| Vehicle Extension (s) |  | 3.0 |  |  |
| Recall Mode |  | Max |  |  |
| v/c Ratio |  | 0.84 |  |  |
| Control Delay |  | 63.1 |  |  |
| Queue Delay |  | 0.0 |  |  |
| Total Delay |  | 63.1 |  |  |
| Queue Length 50th (ft) |  | 69 |  |  |
| Queue Length 95th ( t ) |  | \#173 |  |  |
| Internal Link Dist (ft) |  | 184 |  |  |
| Turn Bay Length (ft) |  |  |  |  |
| Base Capacity (vph) |  | 212 |  |  |
| Starvation Cap Reductn |  | 0 |  |  |


|  | $\rangle$ | $\rightarrow$ | - | 5 | 4 | 4 | 4 | $\uparrow$ | $p$ | $\checkmark$ | 4 | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL2 | WBT | WBR | NBL | NBT | NBR | SBL2 | SBL | SBT |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  |  | 0 |
| Reduced v/c Ratio | 1.21 | 0.98 |  |  | 0.94 |  |  | 0.07 |  |  |  | 1.25 |

Intersection Summary

## Area Type: <br> Other

Cycle Length: 65
Actuated Cycle Length: 65
Natural Cycle: 90
Control Type: Actuated-Uncoordinated
~ Volume exceeds capacity, queue is theoretically infinite. Queue shown is maximum after two cycles.
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: East Main Street \& Preston Avenue


|  | SBR | NWL | NWR |
| :--- | ---: | ---: | ---: |
|  | NWR2 |  |  |
| Lane Group | 0 |  |  |
| Spillback Cap Reductn | 0 |  |  |
| Storage Cap Reductn | 0.84 |  |  |
| Reduced v/c Ratio |  |  |  |
| Intersection Summary |  |  |  |


|  | $\prime$ | $\rightarrow$ | T | K | 4 |  | 4 | $\uparrow$ | $p$ | $\checkmark$ | 4 | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBL | EBT | EBR | WBL2 | WBT | WBR | NBL | NBT | NBR | SBL2 | SBL | SBT |
| Lane Configurations | \% | $\hat{1}$ |  |  | \$ |  |  | $\uparrow$ |  |  |  | $\dagger$ |
| Volume (vph) | 417 | 439 | 166 | 2 | 275 | 50 | 6 | 6 | 6 | 71 | 126 | 0 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) | 2.0 | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  |  | 6.0 |
| Lane Util. Factor | 1.00 | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  |  | 1.00 |
| Fit | 1.00 | 0.96 |  |  | 0.98 |  |  | 0.95 |  |  |  | 0.94 |
| Flt Protected | 0.95 | 1.00 |  |  | 1.00 |  |  | 0.98 |  |  |  | 0.97 |
| Satd. Flow (prot) | 1770 | 1786 |  |  | 1823 |  |  | 1750 |  |  |  | 1707 |
| Flt Permitted | 0.26 | 1.00 |  |  | 0.96 |  |  | 0.87 |  |  |  | 0.81 |
| Satd. Flow (perm) | 483 | 1786 |  |  | 1754 |  |  | 1548 |  |  |  | 1423 |
| Peak-hour factor, PHF | 0.86 | 0.86 | 0.86 | 0.84 | 0.84 | 0.84 | 0.92 | 0.92 | 0.92 | 0.84 | 0.84 | 0.84 |
| Adj. Flow (vph) | 485 | 510 | 193 | 2 | 327 | 60 | 7 | 7 | 7 | 85 | 150 | 0 |
| RTOR Reduction (vph) | 0 | 0 | 0 | 0 | 10 | 0 | 0 | 0 | 0 | 0 | 0 | 41 |
| Lane Group Flow (vph) | 485 | 703 | 0 | 0 | 379 | 0 | 0 | 21 | 0 | 0 | 0 | 368 |
| Tum Type | pm+pt |  |  | Perm |  |  | Perm |  |  | Perm | Perm |  |
| Protected Phases | 7 | 4 |  |  | 8 |  |  | 2 |  |  |  | 6 |
| Permitted Phases | 4 |  |  | 8 |  |  | 2 |  |  | 6 | 6 | 6 |
| Actuated Green, G (s) | 26.0 | 26.0 |  |  | 15.0 |  |  | 13.0 |  |  |  | 13.0 |
| Effective Green, g (s) | 26.0 | 26.0 |  |  | 15.0 |  |  | 13.0 |  |  |  | 13.0 |
| Actuated g/C Ratio | 0.40 | 0.40 |  |  | 0.23 |  |  | 0.20 |  |  |  | 0.20 |
| Clearance Time (s) | 2.0 | 6.0 |  |  | 6.0 |  |  | 6.0 |  |  |  | 6.0 |
| Vehicle Extension (s) | 3.0 | 3.0 |  |  | 3.0 |  |  | 3.0 |  |  |  | 3.0 |
| Lane Grp Cap (vph) | 371 | 714 |  |  | 405 |  |  | 310 |  |  |  | 285 |
| v/s Ratio Prot | c0.18 | c0.39 |  |  |  |  |  |  |  |  |  |  |
| v/s Ratio Perm | 0.34 |  |  |  | 0.22 |  |  | 0.01 |  |  |  | c0. 26 |
| v/c Ratio | 1.31 | 0.98 |  |  | 0.94 |  |  | 0.07 |  |  |  | 1.29 |
| Uniform Delay, d1 | 17.5 | 19.3 |  |  | 24.5 |  |  | 21.1 |  |  |  | 26.0 |
| Progression Factor | 1.00 | 1.00 |  |  | 1.00 |  |  | 1.00 |  |  |  | 1.00 |
| Incremental Delay, d2 | 156.5 | 29.6 |  |  | 28.8 |  |  | 0.4 |  |  |  | 155.0 |
| Delay (s) | 174.1 | 48.9 |  |  | 53.3 |  |  | 21.5 |  |  |  | 181.0 |
| Level of Service | F | D |  |  | D |  |  | C |  |  |  | F |
| Approach Delay (s) |  | 100.0 |  |  | 53.3 |  |  | 21.5 |  |  |  | 181.0 |
| Approach LOS |  | F |  |  | D |  |  | C |  |  |  | F |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 102.8 |  | HCM Leve | of Servic |  |  | F |  |  |  |
| HCM Volume to Capacity ratio |  |  | 1.02 |  |  |  |  |  |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 65.0 |  | Sum of los | time (s) |  |  | 14.0 |  |  |  |
| Intersection Capacity Utilization |  |  | 106.8\% |  | CU Level | Service |  |  | G |  |  |  |
| Analysis Period (min) |  |  | 15 |  |  |  |  |  |  |  |  |  |
| c Critical Lane Group |  |  |  |  |  |  |  |  |  |  |  |  |


|  | $\checkmark$ | * | 4 | $\stackrel{ }{ }+$ |
| :---: | :---: | :---: | :---: | :---: |
| Movement | SBR | NWL | NWR | NWR2 |
| Lan\&Sonfigurations |  | \% |  |  |
| Volume (vph) | 146 | 85 | 68 | 10 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 |
| Total Lost time (s) |  | 6.0 |  |  |
| Lane Util. Factor |  | 1.00 |  |  |
| Fit |  | 0.94 |  |  |
| Flt Protected |  | 0.97 |  |  |
| Satd. Flow (prot) |  | 1698 |  |  |
| Flt Permitted |  | 0.97 |  |  |
| Satd. Flow (perm) |  | 1698 |  |  |
| Peak-hour factor, PHF | 0.84 | 0.91 | 0.91 | 0.91 |
| Adj. Flow (vph) | 174 | 93 | 75 | 11 |
| RTOR Reduction (vph) | 0 | 4 | 0 | 0 |
| Lane Group Flow (vph) | 0 | 175 | 0 | 0 |
| Turn Type |  |  |  |  |
| Protected Phases |  | 5 |  |  |
| Permitted Phases |  | 5 |  |  |
| Actuated Green, G (s) |  | 8.0 |  |  |
| Effective Green, g (s) |  | 8.0 |  |  |
| Actuated g/C Ratio |  | 0.12 |  |  |
| Clearance Time (s) |  | 6.0 |  |  |
| Vehicle Extension (s) |  | 3.0 |  |  |
| Lane Grp Cap (vph) |  | 209 |  |  |
| v/s Ratio Prot |  | c0.10 |  |  |
| v/s Ratio Perm |  |  |  |  |
| v/c Ratio |  | 0.84 |  |  |
| Uniform Delay, d1 |  | 27.9 |  |  |
| Progression Factor |  | 1.00 |  |  |
| Incremental Delay, d2 |  | 31.4 |  |  |
| Delay (s) |  | 59.3 |  |  |
| Level of Service |  | E |  |  |
| Approach Delay (s) |  | 59.3 |  |  |
| Approach LOS |  | E |  |  |
| Intersection Summary |  |  |  |  |


|  | 多 | $\rightarrow$ | V | 1 | 4 | 央 | 4 | $\dagger$ | P | - | $\frac{1}{7}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{\beta}$ |  |  | * |  |  | 4* |  |  | 4 | ${ }^{7}$ |
| Volume (vph) | 146 | 240 | 43 | 1 | 257 | 52 | 61 | 76 | 5 | 35 | 39 | 322 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length (ft) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 100 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  | 25 | 25 |  | 25 | 25 |  | 25 | 25 |  | 50 |
| Lane Util. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Fit |  | 0.977 |  |  | 0.978 |  |  | 0.995 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  |  |  |  |  | 0.979 |  |  | 0.977 |  |
| Satd. Flow (prot) | 1770 | 1820 | 0 | 0 | 1822 | 0 | 0 | 1815 | 0 | 0 | 1820 | 1583 |
| Flt Permitted | 0.421 |  |  |  | 0.999 |  |  | 0.816 |  |  | 0.726 |  |
| Satd. Flow (perm) | 784 | 1820 | 0 | 0 | 1820 | 0 | 0 | 1512 | 0 | 0 | 1352 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 32 |  |  | 16 |  |  | 2 |  |  |  | 424 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 104 |  |  | 913 |  |  | 284 |  |  | 1046 |  |
| Travel Time (s) |  | 2.4 |  |  | 20.8 |  |  | 6.5 |  |  | 23.8 |  |
| Peak Hour Factor | 0.83 | 0.83 | 0.83 | 0.86 | 0.86 | 0.86 | 0.81 | 0.81 | 0.81 | 0.76 | 0.76 | 0.76 |
| Adj. Flow (vph) | 176 | 289 | 52 | 1 | 299 | 60 | 75 | 94 | 6 | 46 | 51 | 424 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 176 | 341 | 0 | 0 | 360 | 0 | 0 | 175 | 0 | 0 | 97 | 424 |
| Turn Type | D.P+P |  |  | Perm |  |  | Perm |  |  | Perm |  | custom |
| Protected Phases | 14 | 124 |  |  | 2 |  |  | 3 |  |  | 3 | 1 |
| Permitted Phases | 2 |  |  | 2 |  |  | 3 | 3 |  | 3 | 3 | 3 |
| Detector Phase | 14 | 124 |  | 2 | 2 |  | 3 | 3 |  | 3 | 3 | 1 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) |  |  |  | 8.0 | 8.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 | 15.0 |
| Minimum Split (s) |  |  |  | 14.0 | 14.0 |  | 14.0 | 14.0 |  | 14.0 | 14.0 | 21.0 |
| Total Split (s) | 27.0 | 56.0 | 0.0 | 29.0 | 29.0 | 0.0 | 14.0 | 14.0 | 0.0 | 14.0 | 14.0 | 13.0 |
| Total Split (\%) | 38.6\% | 80.0\% | 0.0\% | 41.4\% | 41.4\% | 0.0\% | 20.0\% | 20.0\% | 0.0\% | 20.0\% | 20.0\% | 18.6\% |
| Maximum Green (s) |  |  |  | 23.0 | 23.0 |  | 9.0 | 9.0 |  | 9.0 | 9.0 | 7.0 |
| Yellow Time (s) |  |  |  | 4.0 | 4.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 4.0 |
| All-Red Time (s) |  |  |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | -1.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 | 4.0 | 6.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 6.0 |
| Lead/Lag |  |  |  | Lag | Lag |  | Lead | Lead |  | Lead | Lead | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) |  |  |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode |  |  |  | C-Max | C-Max |  | None | None |  | None | None | None |
| v/c Ratio | 0.22 | 0.26 |  |  | 0.57 |  |  | 0.89 |  |  | 0.56 | 0.63 |
| Control Delay | 3.1 | 1.5 |  |  | 22.1 |  |  | 75.3 |  |  | 42.6 | 6.0 |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  | 14.8 |  |  | 0.0 | 1.6 |
| Total Delay | 3.1 | 1.5 |  |  | 22.1 |  |  | 90.0 |  |  | 42.6 | 7.6 |
| Queue Length 50th (ft) | 3 | 0 |  |  | 118 |  |  | 75 |  |  | 40 | 0 |
| Queue Length 95th ( ft ) | 5 | 9 |  |  | 186 |  |  | \#157 |  |  | 70 | 18 |
| Internal Link Dist (ft) |  | 24 |  |  | 833 |  |  | 204 |  |  | 966 |  |
| Turn Bay Length ( ft ) |  |  |  |  |  |  |  |  |  |  |  | 100 |
| Base Capacity (vph) | 736 | 1255 |  |  | 635 |  |  | 196 |  |  | 174 | 677 |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  | 0 | 0 |


| Lane Group | 64 |  |
| :---: | :---: | :---: |
| Lanertonfigurations |  |  |
| Volume (vph) |  |  |
| Ideal Flow (vphpl) |  |  |
| Storage Length (ft) |  |  |
| Storage Lanes |  |  |
| Taper Length (ft) |  |  |
| Lane Util. Factor |  |  |
| Frt |  |  |
| Flt Protected |  |  |
| Satd. Flow (prot) |  |  |
| Flt Permitted |  |  |
| Satd. Flow (perm) |  |  |
| Right Turn on Red |  |  |
| Satd. Flow (RTOR) |  |  |
| Link Speed (mph) |  |  |
| Link Distance ( ft ) |  |  |
| Travel Time (s) |  |  |
| Peak Hour Factor |  |  |
| Adj. Flow (vph) |  |  |
| Shared Lane Traffic (\%) |  |  |
| Lane Group Flow (vph) |  |  |
| Turn Type |  |  |
| Protected Phases | 4 |  |
| Permitted Phases |  |  |
| Detector Phase |  |  |
| Switch Phase |  |  |
| Minimum Initial (s) | 8.0 |  |
| Minimum Split (s) | 14.0 |  |
| Total Split (s) | 14.0 |  |
| Total Split (\%) | 20\% |  |
| Maximum Green (s) | 9.0 |  |
| Yellow Time (s) | 3.0 |  |
| All-Red Time (s) | 2.0 |  |
| Lost Time Adjust (s) |  |  |
| Total Lost Time (s) |  |  |
| Lead/Lag | Lag |  |
| Lead-Lag Optimize? |  |  |
| Vehicle Extension (s) | 3.0 |  |
| $\mathrm{v} / \mathrm{C}$ Ratio |  |  |
| Control Delay |  |  |
| Queue Delay |  |  |
| Total Delay |  |  |
| Queue Length 50th (ft) |  |  |
| Queue Length 95th (ft) |  |  |
| Internal Link Dist (tt) |  |  |
| Turn Bay Length ( ft ) |  |  |
| Base Capacity (vph) |  |  |
| Starvation Cap Reduct |  |  |
| Meriden Road Plannin F\&O | 6/29/2010 Altemate \#1 Future Conditions (2030) | Synchro 7 - Report Page 2 |


|  | 4 | $\rightarrow$ | $\cdots$ | $\checkmark$ | $\leftarrow$ | 4 | 4 | 4 | $p$ |  | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 |  |  | 4 |  |  | 17 |  |  | 0 | 117 |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  | 0 | 0 |
| Reduced v/c Ratio | 0.24 | 0.27 |  |  | 0.57 |  |  | 0.98 |  |  | 0.56 | 0.76 |

Intersection Summary
Area Type:
Other
Cycle Length: 70
Actuated Cycle Length: 70
Offset: $0(0 \%)$, Referenced to phase 2:EBWB, Start of Yellow
Natural Cycle: 70
Control Type: Actuated-Coordinated
\# 95th percentile volume exceeds capacity, queue may be longer.
Queue shown is maximum after two cycles.
Splits and Phases: 1: East Main Street \& Preston Avenue

| $\begin{aligned} & \begin{array}{l} \# 1 \\ \stackrel{\# 1}{4} \\ 4 \end{array} \stackrel{1}{4} \end{aligned}$ | $\stackrel{\# 1}{\leftrightarrows} \stackrel{\# 7}{\leftrightarrows}$ |  | $\begin{aligned} & \# 1 \\ & \stackrel{\# 1}{\# 4} \\ & 4 \end{aligned}$ |
| :---: | :---: | :---: | :---: |
| 13s | 29 s | 14.5 | 14 s |


| Lane Group $\quad \varnothing 4$ |
| :--- |
| Sillback Cap Reductn |
| Storage Cap Reductn |
| Reduced v/c Ratio |
| Intersection Summary |


c Critical Lane Group


## Intersection Summary

Area Type: Other
Cycle Length: 70
Actuated Cycle Length: 70
Offset: 0 (0\%), Referenced to phase 2:EBWB, Start of Yellow
Natural Cycle: 70
Control Type: Actuated-Coordinated
$m$ Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 7: East Main Street \& Pomery Avenue

| $\begin{aligned} & \# 1 \\ & \stackrel{y y}{4} \stackrel{\# 1}{4} \end{aligned}$ | $\stackrel{\# 7}{\#} \stackrel{\# 7}{\leftrightarrows}$ |  | $\left[\begin{array}{l} \# 1 \\ 4 \\ 4 \end{array}\right.$ |
| :---: | :---: | :---: | :---: |
| 13 s | 29 s | 14 s | 14 s |



|  | \% | $\rightarrow$ | 7 | 1 | - | 4 | 4 | $\uparrow$ | > | $\checkmark$ | $\downarrow$ | $\downarrow$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Lane Configurations | \% | $\hat{t}$ |  |  | ¢ |  |  | $\uparrow$ |  |  | $\uparrow$ | F |
| Volume (vph) | 423 | 445 | 166 | 2 | 276 | 50 | 85 | 68 | 10 | 71 | 126 | 147 |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |
| Storage Length ( ft ) | 0 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 100 |
| Storage Lanes | 1 |  | 0 | 0 |  | 0 | 0 |  | 0 | 0 |  | 1 |
| Taper Length (ft) | 25 |  | 25 | 25 |  | 25 | 25 |  | 25 | 25 |  | 50 |
| Lane Utill. Factor | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 | 1.00 |
| Frt |  | 0.959 |  |  | 0.979 |  |  | 0.992 |  |  |  | 0.850 |
| Flt Protected | 0.950 |  |  |  |  |  |  | 0.975 |  |  | 0.982 |  |
| Satd. Flow (prot) | 1770 | 1786 | 0 | 0 | 1824 | 0 | 0 | 1802 | 0 | 0 | 1829 | 1583 |
| Flt Permitted | 0.260 |  |  |  | 0.996 |  |  | 0.500 |  |  | 0.797 |  |
| Satd. Flow (perm) | 484 | 1786 | 0 | 0 | 1816 | 0 | 0 | 924 | 0 | 0 | 1485 | 1583 |
| Right Turn on Red |  |  | Yes |  |  | Yes |  |  | Yes |  |  | Yes |
| Satd. Flow (RTOR) |  | 43 |  |  | 10 |  |  | 3 |  |  |  | 175 |
| Link Speed (mph) |  | 30 |  |  | 30 |  |  | 30 |  |  | 30 |  |
| Link Distance (ft) |  | 104 |  |  | 913 |  |  | 284 |  |  | 1046 |  |
| Travel Time (s) |  | 2.4 |  |  | 20.8 |  |  | 6.5 |  |  | 23.8 |  |
| Peak Hour Factor | 0.88 | 0.88 | 0.88 | 0.86 | 0.86 | 0.86 | 0.91 | 0.91 | 0.91 | 0.84 | 0.84 | 0.84 |
| Adj. Flow (vph) | 481 | 506 | 189 | 2 | 321 | 58 | 93 | 75 | 11 | 85 | 150 | 175 |
| Shared Lane Traffic (\%) |  |  |  |  |  |  |  |  |  |  |  |  |
| Lane Group Flow (vph) | 481 | 695 | 0 | 0 | 381 | 0 | 0 | 179 | 0 | 0 | 235 | 175 |
| Turn Type | D.P+P |  |  | Perm |  |  | Perm |  |  | Perm |  | custom |
| Protected Phases | 14 | 124 |  |  | 2 |  |  |  |  |  | 3 | 1 |
| Permitted Phases | 2 |  |  | 2 |  |  | 3 | 3 |  | 3 | 3 | 3 |
| Detector Phase | 14 | 124 |  | 2 | 2 |  | 3 | 3 |  | 3 | 3 | 1 |
| Switch Phase |  |  |  |  |  |  |  |  |  |  |  |  |
| Minimum Initial (s) |  |  |  | 8.0 | 8.0 |  | 8.0 | 8.0 |  | 8.0 | 8.0 | 15.0 |
| Minimum Split (s) |  |  |  | 14.0 | 14.0 |  | 14.0 | 14.0 |  | 14.0 | 14.0 | 21.0 |
| Total Split (s) | 37.0 | 65.0 | 0.0 | 28.0 | 28.0 | 0.0 | 25.0 | 25.0 | 0.0 | 25.0 | 25.0 | 23.0 |
| Total Split (\%) | 41.1\% | 72.2\% | 0.0\% | 31.1\% | 31.1\% | 0.0\% | 27.8\% | 27.8\% | 0.0\% | 27.8\% | 27.8\% | 25.6\% |
| Maximum Green (s) |  |  |  | 22.0 | 22.0 |  | 20.0 | 20.0 |  | 20.0 | 20.0 | 17.0 |
| Yellow Time (s) |  |  |  | 4.0 | 4.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 4.0 |
| All-Red Time (s) |  |  |  | 2.0 | 2.0 |  | 2.0 | 2.0 |  | 2.0 | 2.0 | 2.0 |
| Lost Time Adjust (s) | 0.0 | 0.0 | 0.0 | 0.0 | -1.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 | 0.0 |
| Total Lost Time (s) | 6.0 | 6.0 | 4.0 | 6.0 | 5.0 | 4.0 | 5.0 | 5.0 | 4.0 | 5.0 | 5.0 | 6.0 |
| Lead/Lag |  |  |  | Lag | Lag |  | Lead | Lead |  | Lead | Lead | Lead |
| Lead-Lag Optimize? |  |  |  |  |  |  |  |  |  |  |  |  |
| Vehicle Extension (s) |  |  |  | 3.0 | 3.0 |  | 3.0 | 3.0 |  | 3.0 | 3.0 | 3.0 |
| Recall Mode |  |  |  | C-Max | C-Max |  | None | None |  | None | None | None |
| v/c Ratio | 0.64 | 0.58 |  |  | 0.81 |  |  | 0.91 |  |  | 0.76 | 0.24 |
| Control Delay | 18.6 | 4.2 |  |  | 45.6 |  |  | 81.2 |  |  | 49.8 | 2.4 |
| Queue Delay | 0.0 | 0.0 |  |  | 0.0 |  |  | 0.0 |  |  | 0.0 | 0.0 |
| Total Delay | 18.6 | 4.2 |  |  | 45.6 |  |  | 81.2 |  |  | 49.8 | 2.4 |
| Queue Length 50th ( ft ) | 79 | 40 |  |  | 198 |  |  | 97 |  |  | 124 | 0 |
| Queue Length 95th (ft) | 163 | 57 |  |  | \#314 |  |  | \#218 |  |  | \#190 | 18 |
| Internal Link Dist (ft) |  | 24 |  |  | 833 |  |  | 204 |  |  | 966 |  |
| Turn Bay Length (tt) |  |  |  |  |  |  |  |  |  |  |  | 100 |
| Base Capacity (vph) | 751 | 1208 |  |  | 472 |  |  | 208 |  |  | 330 | 720 |
| Starvation Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  | 0 | 0 |



|  | \% | $\rightarrow$ | 7 | 7 | 4 | 4 | 4 | $\dagger$ | P | * | $\frac{1}{7}$ | 4 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Lane Group | EBL | EBT | EBR | WBL | WBT | WBR | NBL | NBT | NBR | SBL | SBT | SBR |
| Spillback Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  | 0 | 13 |
| Storage Cap Reductn | 0 | 0 |  |  | 0 |  |  | 0 |  |  | 0 | 0 |
| Reduced v/c Ratio | 0.64 | 0.58 |  |  | 0.81 |  |  | 0.86 |  |  | 0.71 | 0.25 |
| Intersection Summary |  |  |  |  |  |  |  |  |  |  |  |  |

Ansecion
Area Type:

## Other

Cycle Length: 90
Actuated Cycle Length: 90
Offset: 0 (0\%), Referenced to phase 2:EBWB, Start of Yellow
Natural Cycle: 80
Control Type: Actuated-Coordinated
\# 95th percentile volume exceeds capacity, queue may be longer. Queue shown is maximum after two cycles.

Splits and Phases: 1: East Main Street \& Preston Avenue


Lane Group $\quad 64$
Spillback Cap Reductn
Storage Cap Reductn
Reduced v/c Ratio
Intersection Summary

c Critical Lane Group


## Intersection Summary

Area Type: Other
Cycle Length: 90
Actuated Cycle Length: 90
Offset: 0 (0\%), Referenced to phase 2:EBWB, Start of Yellow
Natural Cycle: 80
Control Type: Actuated-Coordinated
m Volume for 95 th percentile queue is metered by upstream signal.
Splits and Phases: 7: East Main Street \& Pomery Avenue


|  | $\rightarrow$ | \% | 1 | 4 | 4 | $p$ |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| Movement | EBT | EBR | WBL | WBT | NBL | NBR |  |
| Lane Configurations | 里 ${ }^{\text {a }}$ |  |  | 4 | * |  |  |
| Volume (vph) | 1022 | 6 | 2 | 506 | 6 | 12 |  |
| Ideal Flow (vphpl) | 1900 | 1900 | 1900 | 1900 | 1900 | 1900 |  |
| Total Lost time (s) | 6.0 |  |  | 6.0 | 5.0 |  |  |
| Lane Util. Factor | 0.95 |  |  | 1.00 | 1.00 |  |  |
| Frt | 1.00 |  |  | 1.00 | 0.91 |  |  |
| Fit Protected | 1.00 |  |  | 1.00 | 0.98 |  |  |
| Satd. Flow (prot) | 3536 |  |  | 1862 | 1670 |  |  |
| Flt Permitted | 1.00 |  |  | 1.00 | 0.98 |  |  |
| Satd. Flow (perm) | 3536 |  |  | 1858 | 1670 |  |  |
| Peak-hour factor, PHF | 0.88 | 0.88 | 0.86 | 0.86 | 0.91 | 0.91 |  |
| Adj. Flow (vph) | 1161 | 7 | 2 | 588 | 7 | 13 |  |
| RTOR Reduction (vph) | 1 | 0 | 0 | 0 | 12 | 0 |  |
| Lane Group Flow (vph) | 1168 | 0 | 0 | 590 | 8 | 0 |  |
| Turn Type |  |  | D.Pm |  |  |  |  |
| Protected Phases | 12 |  |  | 123 | 4 |  |  |
| Permitted Phases |  |  | 12 |  |  |  |  |
| Actuated Green, G (s) | 45.0 |  |  | 69.8 | 10.2 |  |  |
| Effective Green, g (s) | 45.0 |  |  | 69.8 | 10.2 |  |  |
| Actuated g/C Ratio | 0.50 |  |  | 0.78 | 0.11 |  |  |
| Clearance Time (s) |  |  |  |  | 5.0 |  |  |
| Vehicle Extension (s) |  |  |  |  | 3.0 |  |  |
| Lane Grp Cap (vph) | 1768 |  |  | 1441 | 189 |  |  |
| v/s Ratio Prot | c0.33 |  |  |  | c0.01 |  |  |
| v/s Ratio Perm |  |  |  | c0.32 |  |  |  |
| v/c Ratio | 0.66 |  |  | 0.41 | 0.04 |  |  |
| Uniform Delay, d1 | 16.8 |  |  | 3.3 | 35.6 |  |  |
| Progression Factor | 1.00 |  |  | 0.31 | 1.00 |  |  |
| Incremental Delay, d2 | 0.9 |  |  | 0.1 | 0.1 |  |  |
| Delay (s) | 17.7 |  |  | 1.2 | 35.7 |  |  |
| Level of Service | B |  |  | A | D |  |  |
| Approach Delay (s) | 17.7 |  |  | 1.2 | 35.7 |  |  |
| Approach LOS | B |  |  | A | D |  |  |
| Intersection Summary |  |  |  |  |  |  |  |
| HCM Average Control Delay |  |  | 12.4 |  | HCM Level | of Service | B |
| HCM Volume to Capacity ratio |  |  | 0.49 |  |  |  |  |
| Actuated Cycle Length (s) |  |  | 90.0 |  | Sum of lost | time (s) | 11.0 |
| Intersection Capacity UtilizationAnalysis Period (min) |  |  | 44.3\% |  | ICU Level | Service | A |
|  |  |  | 15 |  |  |  |  |

c Critical Lane Group

## Appendix D

Construction Cost Estimates

| FUSS \& O'NEILL <br> Disciplines to Deliver | 146 Hartford Road Manchester, CT Phone: (860) 646-2469 www.fando.com |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| ORDER OF MAGNITUDE OPINION OF COST |  |  |  |  |
| PROJECT: PRESTON AVENUE/BALDWIN AVENUE CORRIDOR STUDY | DATE PREPARED: 06/18/2010 |  |  |  |
| LOCATION: PRESTON AVENUE | BASIS: ConnDOT 2010 |  |  |  |
| DESCRIPTION: BETWEEN EAST MAIN STREET AND | From Sta. |  | To Sta. |  |
| PARKER ROAD - ALTERNATIVE \#1 | LENGTH: 1,150 |  | WIDTH: 26 |  |
| PROJECT NO.: 20090602.A10 | ESTIMLATOR: SNB/MSR |  | CHECKED BY: KPC |  |
| Since Fuss \& O'Neill has no control over the cost of labor, materials, equipment or services furnished by others, or over the Contractor(s') methods of determining prices, or over competitive bidding or market conditions, Fuss \& O'Neill's opinion of probable Total Project Costs and Construction Cost are made on the basis of Fuss \& O'Neill's experience and qualifications and represent Fuss \& O'Neill's best judgment as an experienced and qualified professional engineer, familiar with the construction industry; but Fuss \& O'Neill cannot and does not guarantee that proposals, bids or actual Total Project or Construction Costs will not vary from opinions of probable cost prepared by Fuss \& O'Neill. If prior to the bidding or negotiating Phase the Owner wishes greater assurance as to Total Project or Construction Costs, the Owner shall employ an independent cost estimator. |  |  |  |  |
| Item | Est. Quant. | Unit | Unit Price | Total |
| ROADWAY ITEMS |  |  |  |  |
| Earth Excavation | 4300 | c.y. | \$25.00 | \$107,500 |
| Rock Excavation | 25 | c.y. | \$90.00 | \$2,250 |
| Trench Excavation 0-4' Deep | 590 | c.y. | \$20.00 | \$11,800 |
| Trench Excavation 0-10' Deep | 240 | c. y . | \$25.00 | \$6,000 |
| Rock in Trench Excavation | 45 | c.y. | \$150.00 | \$6,750 |
| Subbase | 2350 | c.y. | \$38.00 | \$89,300 |
| Sedimentation Control System | 2400 | I.f. | \$4.00 | \$9,600 |
| H.M.A. | 3490 | ton | \$100.00 | \$349,000 |
| Bedding Material | 90 | c.y. | \$35.00 | \$3,150 |
| 12" R.C.P. | 375 | I.f. | \$55.00 | \$20,625 |
| 15" R.C.P. | 600 | I.f. | \$65.00 | \$39,000 |
| 18" R.C.P. | 300 | I.f. | \$75.00 | \$22,500 |
| 6" P.V.C. Underdrain | 1100 | I.f. | \$30.00 | \$33,000 |
| Simple Catch Basin | 12 | ea. | \$3,000.00 | \$36,000 |
| Structure Resetting (Storm and Sanitary) | 2 | ea. | \$1,000.00 | \$2,000 |
| Bituminous Concrete Lip Curbing | 2850 | I.f. | \$7.00 | \$19,950 |
| Concrete Sidewalk | 5500 | s.f. | \$14.00 | \$77,000 |
| Bituminous Concrete Driveway - Residential | 400 | s.y. | \$40.00 | \$16,000 |
| Furnishing and Placing Topsoil | 1350 | s.y. | \$8.00 | \$10,800 |
| Turf Establishment | 1350 | s.y. | \$3.00 | \$4,050 |
| TRAFFIC ITEMS |  |  |  |  |
| Trafficmen - Town (City) Police Officer | 640 | hr. | \$75.00 | \$48,000 |
| Trafficmen - Uniformed Flagger | 1280 | hr. | \$55.00 | \$70,400 |
| New Signal | 2 | ea. | \$110,000.00 | \$220,000 |
| Contract Items | SUBTOTAL |  |  | \$1,204,700 |
| Clearing and Grubbing Roadway | 2.0\% |  |  | \$24,100 |
| M \& P of Traffic | 4.0\% |  |  | \$48,200 |
| Mobilization | 7.5\% |  |  | \$90,400 |
| Construction Staking | 1.0\% |  |  | \$12,000 |
| Minor Items | 25.0\% |  |  | \$301,200 |
| Inflation Factor | 5.0\% |  |  | \$0 |
|  | CONSTRUCTION TOTALS |  |  | \$1,680,000 |
| CONTINGENCIES |  |  |  | \$168,000 |
| INCIDENTALS | 25.0\% |  |  | \$420,000 |
| UTILITIES | 15.0\% |  |  | \$252,000 |
| RIGHTS OF WAY |  |  |  | \$100,000 |
|  | TOTAL ESTIMATED COST |  |  | \$2,620,000 |


| FUSS \& O'NEILL <br> Disciplines to Deliver | 146 Hartford Road <br> Manchester, CT <br> Phone: (860) 646-2469 <br> www.fando.com |  |  |  |
| :---: | :---: | :---: | :---: | :---: |
| ORDER OF MAGNITUDE OPINION OF COST |  |  |  |  |
| PROJECT: PRESTON AVENUE/BALDWIN AVENUE CORRIDOR STUDY | DATE PREPARED: 06/18/2010 |  |  |  |
| LOCATION: PRESTON AVENUE | BASIS: ConnDOT 2010 |  |  |  |
| DESCRIPTION: BETWEEN EAST MAIN STREET AND | From Sta. |  | To Sta. |  |
| PARKER ROAD - ALTERNATIVE \#2 | LENGTH: 1,150 |  | WIDTH: 26 |  |
| PROJECT NO.: $20090602 . A 10$ | ESTIMATOR: SNB/MSR |  | CHECKED BY: KPC |  |
| Since Fuss \& O'Neill has no control over the cost of labor, materials, equipment or services furnished by others, or over the Contractor(s') methods of determining prices, or over competitive bidding or market conditions, Fuss \& O'Neill's opinion of probable Total Project Costs and Construction Cost are made on the basis of Fuss \& O'Neill's experience and qualifications and represent Fuss \& O'Neill's best judgment as an experienced and qualified professional engineer, familiar with the construction industry; but Fuss \& O'Neill cannot and does not guarantee that proposals, bids or actual Total Project or Construction Costs will not vary from opinions of probable cost prepared by Fuss \& O'Neill. If prior to the bidding or negotiating Phase the Owner wishes greater assurance as to Total Project or Construction Costs, the Owner shall employ an independent cost estimator. |  |  |  |  |
| Item | Est. Quant. Unit |  | Unit Price | Total |
| ROADWAY ITEMS |  |  |  |  |
| Earth Excavation | 4500 | c.y. | \$25.00 | \$112,500 |
| Rock Excavation | 25 | c.y. | \$90.00 | \$2,250 |
| Trench Excavation 0-4' Deep | 590 | c.y. | \$20.00 | \$11,800 |
| Trench Excavation 0-10' Deep | 240 | c.y. | \$25.00 | \$6,000 |
| Rock in Trench Excavation | 45 | c.y. | \$150.00 | \$6,750 |
| Subbase | 2400 | c.y. | \$38.00 | \$91,200 |
| Sedimentation Control System | 2400 | l.f. | \$4.00 | \$9,600 |
| H.M.A. | 3570 | ton | \$100.00 | \$357,000 |
| Bedding Material | 90 | c.y. | \$35.00 | \$3,150 |
| 12" R.C.P. | 375 | I.f. | \$55.00 | \$20,625 |
| $15^{\prime \prime}$ R.C.P. | 600 | I.f. | \$65.00 | \$39,000 |
| 18" R.C.P. | 300 | I.f. | \$75.00 | \$22,500 |
| 6" P.V.C. Underdrain | 1100 | I.f. | \$30.00 | \$33,000 |
| Simple Catch Basin | 12 | ea. | \$3,000.00 | \$36,000 |
| Structure Resetting (Storm and Sanitary) | 2 | ea. | \$1,000.00 | \$2,000 |
| Bituminous Concrete Lip Curbing | 2850 | I.f. | \$7.00 | \$19,950 |
| Concrete Sidewalk | 5500 | s.f. | \$14.00 | \$77,000 |
| Bituminous Concrete Driveway - Residential | 400 | s.y. | \$40.00 | \$16,000 |
| Furnishing and Placing Topsoil | 1350 | s.y. | \$8.00 | \$10,800 |
| Turf Establishment | 1350 | s.y. | \$3.00 | \$4,050 |
| TRAFFIC ITEMS |  |  |  |  |
| Trafficmen - Town (City) Police Officer | 640 | hr. | \$75.00 | \$48,000 |
| Trafficmen - Uniformed Flagger | 1280 | hr | \$55.00 | \$70,400 |
| New Signal | 1 | ea. | \$110,000.00 | \$110,000 |
| Contract Items |  |  | SUBTOTAL | \$1,109,600 |
| Clearing and Grubbing Roadway |  |  |  | \$22,200 |
| M \& P of Traffic | 2.0\% |  |  | \$44,400 |
| Mobilization | 7.5\% |  |  | \$83,200 |
| Construction Staking | 1.0\% |  |  | \$11,100 |
| Minor Items | 25.0\% |  |  | \$277,400 |
| Inflation Factor | 5.0\% |  |  | \$0 |
|  | CONSTRUCTION TOTALS |  |  | \$1,550,000 |
| CONTINGENCIES | 10.0\% |  |  | \$155,000 |
| INCIDENTALS | 25.0\% |  |  | \$388,000 |
| UTILITIES | 15.0\% |  |  | \$233,000 |
| RIGHTS OF WAY |  |  |  | \$500,000 |
|  | TOTAL ESTIMATED COST |  |  | \$2,826,000 |

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## ORDER OF MAGNITUDE OPINION OF COST

PROJECT: PRESTON AVENUE/BALDWIN AVENUE CORRIDOR STUDY

DATE PREPARED: 06/18/2010
LOCATION: PRESTON AVENUE
BASIS: ConnDOT 2010
DESCRIPTION: BETWEEN PARKER ROAD AND ROUTE 66 From Sta. $\quad$ To Sta.
OFF-RAMP
LENGTH: 750 WIDTH: 26
PROJECT NO.: 20090602.A10
ESTIMATOR: SNB/MSR CHECKED BY: KPC
Since Fuss \& O'Neill has no control over the cost of labor, materials, equipment or services furnished by others, or over the Contractor(s') methods of determining prices, or over competitive bidding or market conditions, Fuss \& O'Neill's opinion of probable Total Project Costs and Construction Cost are made on the basis of Fuss \& O'Neill's experience and qualifications and represent Fuss \& O'Neill's best judgment as an experienced and qualified professional engineer, familiar with the construction industry; but Fuss \& O'Neill cannot and does not guarantee that proposals, bids or actual Total Project or Construction Costs will not vary from opinions of probable cost prepared by Fuss \& O'Neill. If prior to the bidding or negotiating Phase the Owner wishes greater assurance as to Total Project or Construction Costs, the Owner shall employ an independent cost estimator.

| Item | Est. Quant. | Unit | Unit Price | Total |
| :---: | :---: | :---: | :---: | :---: |
| ROADWAY ITEMS |  |  |  |  |
| Earth Excavation | 1900 | c.y. | \$25.00 | \$47,500 |
| Trench Excavation 0-4' Deep | 15 | c.y. | \$20.00 | \$300 |
| Trench Excavation 0-10' Deep | 25 | c.y. | \$25.00 | \$625 |
| Subbase | 1080 | c.y. | \$38.00 | \$41,040 |
| Sedimentation Control System | 1500 | I.f. | \$4.00 | \$6,000 |
| H.M.A. | 1600 | ton | \$100.00 | \$160,000 |
| Bedding Material | 2 | c.y. | \$35.00 | \$70 |
| 12" R.C.P. | 25 | I.f. | \$55.00 | \$1,375 |
| 6" P.V.C. Underdrain | 750 | I.f. | \$30.00 | \$22,500 |
| Simple Catch Basin | 1 | ea. | \$3,000.00 | \$3,000 |
| Structure Resetting (Storm and Sanitary) | 2 | ea. | \$1,000.00 | \$2,000 |
| Bituminous Concrete Lip Curbing | 1725 | I.f. | \$7.00 | \$12,075 |
| Metal Beam Rail (Type R-B 350) | 240 | I.f. | \$30.00 | \$7,200 |
| R-B End Anchorage Type I | 1 | ea. | \$1,200.00 | \$1,200 |
| Tangential Impact Attenuator | 1 | ea. | \$4,000.00 | \$4,000 |
| Concrete Sidewalk | 1250 | s.f. | \$14.00 | \$17,500 |
| Bituminous Concrete Driveway - Residential | 350 | s.y. | \$40.00 | \$14,000 |
| Furnishing and Placing Topsoil | 850 | s.y. | \$8.00 | \$6,800 |
| Turf Establishment | 850 | s.y. | \$3.00 | \$2,550 |
| TRAFFIC ITEMS |  |  |  |  |
| Trafficmen - Town (City) Police . Officer | 240 | hr. | \$75.00 | \$18,000 |
| Trafficmen - Uniformed Flagger | 480 | hr. | \$55.00 | \$26,400 |
| Contract Items |  |  | SUBTOTAL | \$394,100 |
| Clearing and Grubbing Roadway |  | 2.0\% |  | \$7,900 |
| $M$ \& $P$ of Traffic |  | 4.0\% |  | \$15,800 |
| Mobilization |  | 7.5\% |  | \$29,600 |
| Construction Staking |  | 1.0\% |  | \$3,900 |
| Minor Items |  | 25.0\% |  | \$98,500 |
| Inflation Factor | 0 | 5.0\% |  | \$0 |
|  |  | CONSTRUCTION TOTALS |  | \$550,000 |
| CONTINGENCIES |  | 10.0\% |  | \$55,000 |
| INCIDENTALS |  | 30.0\% |  | \$165,000 |
| UTILITIES |  | 15.0\% |  | \$83,000 |
|  |  | TOTAL | MATED COST | \$853,000 |

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## ORDER OF MAGNITUDE OPINION OF COST

## PROJECT: PRESTON AVENUE/BALDWIN AVENUE

CORRIDOR STUDY
LOCATION: PRESTON AVENUE
DATE PREPARED: 06/18/2010
BASIS: ConnDOT 2010

| DESCRIPTION: ROUTE 66 OFF-RAMP TO PATTON DRIVE | From Sta. | To Sta. |
| :--- | :--- | :--- |
|  | LENGTH: 2,450 | WIDTH: 26 |
| PROJECT NO:: 20090602.A10 | ESTIMCATOR: SNB/MSR | CHECKED BY: KPC |

Since Fuss \& O'Neill has no control over the cost of labor, materials, equipment or services furnished by others, or over the Contractor(s') methods of determining prices, or over competitive bidding or market conditions, Fuss \& O'Neill's opinion of probable Total Project Costs and Construction Cost are made on the basis of Fuss \& O'Neill's experience and qualifications and represent Fuss \& O'Neill's best judgment as an experienced and qualified professional engineer, familiar with the construction industry; but Fuss \& O'Neill cannot and does not guarantee that proposals, bids or actual Total Project or Construction Costs will not vary from opinions of probable cost prepared by Fuss \& O'Neill. If prior to the bidding or negotiating Phase the Owner wishes greater assurance as to Total Project or Construction Costs, the Owner shall employ an independent cost estimator.

| Item | Est. Quant. | Unit | Unit Price | Total |
| :---: | :---: | :---: | :---: | :---: |
| ROADWAY ITEMS |  |  |  |  |
| Earth Excavation | 4650 | c. y . | \$25.00 | \$116,250 |
| Trench Excavation 0-4' Deep | 950 | c.y. | \$20.00 | \$19,000 |
| Trench Excavation 0-10' Deep | 310 | c.y. | \$25.00 | \$7,750 |
| Rock in Trench Excavation | 65 | c.y. | \$150.00 | \$9,750 |
| Subbase | 2470 | c.y. | \$38.00 | \$93,860 |
| Sedimentation Control System | 4900 | I.f. | \$4.00 | \$19,600 |
| Milling of Bituminous Concrete Pavement | 1700 | s.y. | \$7.50 | \$12,750 |
| H.M.A. | 3850 | ton | \$100.00 | \$385,000 |
| Bedding Material | 150 | c.y. | \$35.00 | \$5,250 |
| 12" R.C.P. | 825 | I.f. | \$55.00 | \$45,375 |
| 15" R.C.P. | 875 | I.f. | \$65.00 | \$56,875 |
| 24" R.C.P. | 350 | I.f. | \$100.00 | \$35,000 |
| 6" P.V.C. Underdrain | 1900 | I.f. | \$30.00 | \$57,000 |
| Simple Catch Basin | 14 | ea. | \$3,000.00 | \$42,000 |
| Double Catch Basin | 2 | ea. | \$3,500.00 | \$7,000 |
| Structure Resetting (Storm and Sanitary) | 15 | ea. | \$1,000.00 | \$15,000 |
| Bituminous Concrete Lip Curbing | 4000 | I.f. | \$7.00 | \$28,000 |
| Metal Beam Rail (Type R-B 350) | 700 | I.f. | \$30.00 | \$21,000 |
| R-B End Anchorage Type I | 1 | ea. | \$1,200.00 | \$1,200 |
| Tangential Impact Attenuator | 2 | ea. | \$4,000.00 | \$8,000 |
| Bituminous Concrete Driveway - Residential | 180 | s.y. | \$40.00 | \$7,200 |
| Furnishing and Placing Topsoil | 2750 | s.y. | \$8.00 | \$22,000 |
| Turf Establishment | 2750 | s.y. | \$3.00 | \$8,250 |
| TRAFFIC ITEMS |  |  |  |  |
| Trafficmen - Town (City) Police Officer | 640 | hr. | \$75.00 | \$48,000 |
| Trafficmen - Uniformed Flagger | 1280 | hr . | \$55.00 | \$70,400 |
| Contract Items |  |  | SUBTOTAL | \$1,141,500 |
| Clearing and Grubbing Roadway |  | 2.0\% |  | \$22,800 |
| $M$ \& P of Traffic |  | 4.0\% |  | \$45,700 |
| Mobilization |  | 7.5\% |  | \$85,600 |
| Construction Staking |  | 1.0\% |  | \$11,400 |
| Minor Items |  | 25.0\% |  | \$285,400 |
| Inflation Factor | 0 | 5.0\% |  | \$0 |
|  |  | CONSTRUCTION TOTALS |  | \$1,590,000 |
| CONTINGENCIES |  | 10.0\% |  | \$159,000 |
| INCIDENTALS |  | 25.0\% |  | \$398,000 |
| UTILITIES |  | 15.0\% |  | \$239,000 |
|  |  | TOTAL | MATED COST | \$2,386,000 |

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## ORDER OF MAGNITUDE OPINION OF COST

| PROJECT: PRESTON AVENUE/BALDWIN AVENUE <br> CORRIDOR STUDY |  |  |
| :--- | :--- | :--- |
| LOCATION: PRESTON AVENUE |  |  |
| DESCRIPTION: PATTON DRIVE TO BALDWIN AVENUE |  | From Sta. |
|  | LENGTH: 1,650 | To Sta. |
| PROJECT NO.: $20090602 . A 10$ | ESTIMATOR: SNB/MSR | CHIDTH: 26 |

Since Fuss \& O'Neill has no control over the cost of labor, materials, equipment or services furnished by others, or over the Contractor(s') methods of determining prices, or over competitive bidding or market conditions, Fuss \& O'Neill's opinion of probable Total Project Costs and Construction Cost are made on the basis of Fuss \& O'Neill's experience and qualifications and represent Fuss \& O'Neill's best judgment as an experienced and qualified professional engineer, familiar with the construction industry; but Fuss \& O'Neill cannot and does not guarantee that proposals, bids or actual Total Project or Construction Costs will not vary from opinions of probable cost prepared by Fuss \& O'Neill. If prior to the bidding or negotiating Phase the Owner wishes greater assurance as to Total Project or Construction Costs, the Owner shall employ an independent cost estimator.

| Item | Est. Quant. | Unit | Unit Price | Total |
| :---: | :---: | :---: | :---: | :---: |
| ROADWAY ITEMS |  |  |  |  |
| Earth Excavation | 3750 | c.y. | \$25.00 | \$93,750 |
| Trench Excavation 0-4' Deep | 500 | c.y. | \$20.00 | \$10,000 |
| Trench Excavation 0-10' Deep | 300 | c.y. | \$25.00 | \$7,500 |
| Subbase | 2125 | c.y. | \$38.00 | \$80,750 |
| Sedimentation Control System | 3300 | I.f. | \$4.00 | \$13,200 |
| H.M.A. | 3160 | ton | \$100.00 | \$316,000 |
| Bedding Material | 75 | c.y. | \$35.00 | \$2,625 |
| 15" R.C.P. | 1000 | I.f. | \$65.00 | \$65,000 |
| 18" R.C.P. | 25 | I.f. | \$75.00 | \$1,875 |
| 6" P.V.C. Underdrain | 1600 | 1.f. | \$30.00 | \$48,000 |
| Simple Catch Basin | 12 | ea. | \$3,000.00 | \$36,000 |
| Double Catch Basin | 2 | ea. | \$3,500.00 | \$7,000 |
| Structure Resetting (Storm and Sanitary) | 6 | ea. | \$1,000.00 | \$6,000 |
| Bituminous Concrete Lip Curbing | 3100 | I.f. | \$7.00 | \$21,700 |
| Metal Beam Rail (Type R-B 350) | 480 | I.f. | \$30.00 | \$14,400 |
| R-B End Anchorage Type I | 2 | ea. | \$1,200.00 | \$2,400 |
| Bituminous Concrete Driveway - Residential | 350 | s.y. | \$40.00 | \$14,000 |
| Furnishing and Placing Topsoil | 1850 | s.y. | \$8.00 | \$14,800 |
| Turf Establishment | 1850 | s.y. | \$3.00 | \$5,550 |
| TRAFFIC ITEMS |  |  |  |  |
| Trafficmen - Town (City) Police Officer | 480 | hr. | \$75.00 | \$36,000 |
| Trafficmen - Uniformed Flagger | 960 | hr . | \$55.00 | \$52,800 |
| Contract Items |  |  | SUBTOTAL | \$849,400 |
| Clearing and Grubbing Roadway |  | 2.0\% |  | \$17,000 |
| $M$ \& P of Traffic |  | 4.0\% |  | \$34,000 |
| Mobilization |  | 7.5\% |  | \$63,700 |
| Construction Staking |  | 1.0\% |  | \$8,500 |
| Minor Items |  | 25.0\% |  | \$212,400 |
| Inflation Factor | 0 | 5.0\% |  | \$0 |
|  |  | CONSTRUCTION TOTALS |  | \$1,190,000 |
| CONTINGENCIES |  | 10.0\% |  | \$119,000 |
| INCIDENTALS |  | 25.0\% |  | \$298,000 |
| UTILITIES |  | 15.0\% |  | \$179,000 |
|  |  | TOTAL | ATED COST | \$1,786,000 |

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# ORDER OF MAGNITUDE OPINION OF COST 

PROJECT: PRESTON AVENUE/BALDWIN AVENUE CORRIDOR STUDY

DATE PREPARED: 06/18/2010
LOCATION: BALDWIN AVENUE
DESCRIPTION: PRESTON AVENUE TO PRESTON DRIVE
BASIS: ConnDOT 2010

| From Sta. | To Sta. |
| :--- | :--- |
| LENGTH: 1,200 | WIDTH: 24 |
| ESTIMLATOR: SNB/MSR | CHECKED BY: KPC |

PROJECT NO.: 20090602.A10
ESTIMLATOR: SNB/MSR $\quad$ CHECKED BY: KPC
Since Fuss \& O'Neill has no control over the cost of labor, materials, equipment or services furnished by others, or over the Contractor(s') methods of determining prices, or over competitive bidding or market conditions, Fuss \& O'Neill's opinion of probable Total Project Costs and Construction Cost are made on the basis of Fuss \& O'Neill's experience and qualifications and represent Fuss \& O'Neill's best judgment as an experienced and qualified professional engineer, familiar with the construction industry; but Fuss \& O'Neill cannot and does not guarantee that proposals, bids or actual Total Project or Construction Costs will not vary from opinions of probable cost prepared by Fuss \& O'Neill. If prior to the bidding or negotiating Phase the Owner wishes greater assurance as to Total Project or Construction Costs, the Owner shall employ an independent cost estimator.

| Item | Est. Quant. | Unit | Unit Price | Total |
| :---: | :---: | :---: | :---: | :---: |
| ROADWAY ITEMS |  |  |  |  |
| Trench Excavation 0-4' Deep | 20 | c.y. | \$20.00 | \$400 |
| Trench Excavation 0-10' Deep | 25 | c.y. | \$25.00 | \$625 |
| Sedimentation Control System | 2400 | I.f. | \$4.00 | \$9,600 |
| Milling of Bituminous Concrete Pavement | 5500 | s.y. | \$7.50 | \$41,250 |
| H.M.A. | 650 | ton | \$100.00 | \$65,000 |
| Bedding Material | 5 | c.y. | \$35.00 | \$175 |
| 12" R.C.P. | 40 | I.f. | \$55.00 | \$2,200 |
| Simple Catch Basin | 1 | ea. | \$3,000.00 | \$3,000 |
| Structure Resetting (Storm and Sanitary) | 12 | ea. | \$1,000.00 | \$12,000 |
| Bituminous Concrete Lip Curbing | 1280 | I.f. | \$7.00 | \$8,960 |
| Metal Beam Rail (Type R-B 350) | 470 | I.f. | \$30.00 | \$14,100 |
| R-B End Anchorage Type I | 4 | ea. | \$1,200.00 | \$4,800 |
| Concrete Sidewalk | 5500 | s.f. | \$14.00 | \$77,000 |
| Bituminous Concrete Driveway - Residential | 200 | s.y. | \$40.00 | \$8,000 |
| Furnishing and Placing Topsoil | 1230 | s.y. | \$8.00 | \$9,840 |
| Turf Establishment | 1230 | s.y. | \$3.00 | \$3,690 |
| TRAFFIC ITEMS |  |  |  |  |
| Trafficmen - Town (City) Police Officer | 160 | hr. | \$75.00 | \$12,000 |
| Trafficmen - Uniformed Flagger | 320 | hr. | \$55.00 | \$17,600 |
| Contract Items |  |  | SUBTOTAL | \$290,200 |
| Clearing and Grubbing Roadway |  | 2.0\% |  | \$5,800 |
| $M$ \& P of Traffic |  | 4.0\% |  | \$11,600 |
| Mobilization |  | 7.5\% |  | \$21,800 |
| Construction Staking |  | 1.0\% |  | \$2,900 |
| Minor Items |  | 25.0\% |  | \$72,600 |
| Inflation Factor | 0 | 5.0\% |  | \$0 |
|  |  | CONSTRUCTION TOTALS |  | \$400,000 |
| CONTINGENCIES |  | 10.0\% |  | \$40,000 |
| INCIDENTALS |  | 30.0\% |  | \$120,000 |
| UTILITIES |  | 15.0\% |  | \$60,000 |
|  |  | TOTAL | MATED COST | \$620,000 |

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# ORDER OF MAGNITUDE OPINION OF COST 

PROJECT: PRESTON AVENUE/BALDWIN AVENUE

CORRIDOR STUDY
LOCATION: BALDWIN AVENUE
DESCRIPTION: PRESTON DRIVE TO HIGBY DRIVE

DATE PREPARED: 06/18/2010
BASIS: ConnDOT 2010

| From Sta. | To Sta. |
| :--- | :--- |

LENGTH: 1,350
ESTIMATOR: SNB/MSR

WIDTH: 24
CHECKED BY: KPC

PROJECT NO.: 20090602.A10
materials, equipment or services furnished by others, or over the Contractor(s') methods of determining prices, or over competitive bidding or market conditions, Fuss \& O'Neill's opinion of probable Total Project Costs and Construction Cost are made on the basis of Fuss \& O'Neill's experience and qualifications and represent Fuss \& O'Neill's best judgment as an experienced and qualified professional engineer, familiar with the construction industry; but Fuss \& O'Neill cannot and does not guarantee that proposals, bids or actual Total Project or Construction Costs will not vary from opinions of probable cost prepared by Fuss \& O'Neill. If prior to the bidding or negotiating Phase the Owner wishes greater assurance as to Total Project or Construction Costs, the Owner shall employ an independent cost estimator.

| Item | Est. Quant. | Unit | Unit Price | Total |
| :---: | :---: | :---: | :---: | :---: |
| ROADWAY ITEMS |  |  |  |  |
| Earth Excavation | 1100 | c.y. | \$25.00 | \$27,500 |
| Trench Excavation 0-4' Deep | 350 | c.y. | \$20.00 | \$7,000 |
| Trench Excavation 0-10' Deep | 175 | c.y. | \$25.00 | \$4,375 |
| Subbase | 675 | c.y. | \$38.00 | \$25,650 |
| Sedimentation Control System | 2700 | I.f. | \$4.00 | \$10,800 |
| Milling of Bituminous Concrete Pavement | 1700 | s.y. | \$7.50 | \$12,750 |
| H.M.A. | 1440 | ton | \$100.00 | \$144,000 |
| Bedding Material | 50 | c.y. | \$35.00 | \$1,750 |
| 12" R.C.P. | 75 | I.f. | \$55.00 | \$4,125 |
| 15" R.C.P. | 575 | I.f. | \$65.00 | \$37,375 |
| 18" R.C.P. | 50 | I.f. | \$75.00 | \$3,750 |
| Simple Catch Basin | 8 | ea. | \$3,000.00 | \$24,000 |
| Structure Resetting (Storm and Sanitary) | 5 | ea. | \$1,000.00 | \$5,000 |
| Bituminous Concrete Lip Curbing | 2570 | I.f. | \$7.00 | \$17,990 |
| Concrete Curbing | 100 | I.f. | \$35.00 | \$3,500 |
| Concrete Sidewalk | 9350 | s.f. | \$14.00 | \$130,900 |
| Bituminous Concrete Driveway - Residential | 275 | s.y. | \$40.00 | \$11,000 |
| Furnishing and Placing Topsoil | 1500 | s.y. | \$8.00 | \$12,000 |
| Turf Establishment | 1500 | s.y. | \$3.00 | \$4,500 |
| TRAFFIC ITEMS |  |  |  |  |
| Trafficmen - Town (City) Police Officer | 320 | hr. | \$75.00 | \$24,000 |
| Trafficmen - Uniformed Flagger | 640 | hr. | \$55.00 | \$35,200 |
| Contract Items |  |  | SUBTOTAL | \$547,200 |
| Clearing and Grubbing Roadway |  | 2.0\% |  | \$10,900 |
| $M \& P$ of Traffic |  | 4.0\% |  | \$21,900 |
| Mobilization |  | 7.5\% |  | \$41,000 |
| Construction Staking |  | 1.0\% |  | \$5,500 |
| Minor Items |  | 25.0\% |  | \$136,800 |
| Inflation Factor | 0 | 5.0\% |  | \$0 |
|  |  | CONSTRUCTION TOTALS |  | \$760,000 |
| CONTINGENCIES |  | 10.0\% |  | \$76,000 |
| INCIDENTALS |  | 30.0\% |  | \$228,000 |
| UTILITIES |  | 15.0\% |  | \$114,000 |
|  |  | TOTAL E | MATED COST | \$1,178,000 |

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## ORDER OF MAGNITUDE OPINION OF COST

## PROJECT: PRESTON AVENUE/BALDWIN AVENUE CORRIDOR STUDY

LOCATION: BALDWIN AVENUE
DESCRIPTION: HIGBY DRIVE TO BEE STREET

DATE PREPARED: 06/18/2010
BASIS: ConnDOT 2010

| From Sta. | To Sta. |
| :--- | :--- |
| LENGTH: 1,450 | WIDTH: 24 |
| ESTIMLATOR: SNB/MSR | CHECKED BY: KPC |

Since Fuss \& O'Neill has no control over the cost of labor, materials, equipment or services furnished by others, or over the Contractor(s') methods of determining prices, or over competitive bidding or market conditions, Fuss \& O'Neill's opinion of probable Total Project Costs and Construction Cost are made on the basis of Fuss \& O'Neill's experience and qualifications and represent Fuss \& O'Neill's best judgment as an experienced and qualified professional engineer, familiar with the construction industry; but Fuss \& O'Neill cannot and does not guarantee that proposals, bids or actual Total Project or Construction Costs will not vary from opinions of probable cost prepared by Fuss \& O'Neill. If prior to the bidding or negotiating Phase the Owner wishes greater assurance as to Total Project or Construction Costs, the Owner shall employ an independent cost estimator.

| Item | Est. Quant. | Unit | Unit Price | Total |
| :---: | :---: | :---: | :---: | :---: |
| ROADWAY ITEMS |  |  |  |  |
| Earth Excavation | 1900 | c.y. | \$25.00 | \$47,500 |
| Trench Excavation 0-4' Deep | 520 | c.y. | \$20.00 | \$10,400 |
| Trench Excavation 0-10' Deep | - 340 | c. y . | \$25.00 | \$8,500 |
| Trench Excavation 0-15' Deep | 0 | c.y. | \$40.00 | \$0 |
| Subbase | 910 | c.y. | \$38.00 | \$34,580 |
| Sedimentation Control System | 2900 | l.f. | \$4.00 | \$11,600 |
| Milling of Bituminous Concrete Pavement | 920 | s.y. | \$7.50 | \$6,900 |
| H.M.A. | 1810 | ton | \$100.00 | \$181,000 |
| Bedding Material | 75 | c.y. | \$35.00 | \$2,625 |
| 15" R.C.P. | 1050 | I.f. | \$65.00 | \$68,250 |
| Simple Catch Basin | 14 | ea. | \$3,000.00 | \$42,000 |
| Manhole | 2 | ea. | \$3,000.00 | \$6,000 |
| Structure Resetting (Storm and Sanitary) | 8 | ea. | \$1,000.00 | \$8,000 |
| Bituminous Concrete Lip Curbing | 1350 | I.f. | \$7.00 | \$9,450 |
| Concrete Curbing | 1350 | I.f. | \$35.00 | \$47,250 |
| Concrete Sidewalk | 7500 | s.f. | \$14.00 | \$105,000 |
| Bituminous Concrete Driveway - Residential | 550 | s.y. | \$40.00 | \$22,000 |
| Furnishing and Placing Topsoil | 1625 | s.y. | \$8.00 | \$13,000 |
| Turf Establishment | 1625 | s.y. | \$3.00 | \$4,875 |
| Stone Retaining Wall (From Baldwin Ave Improv. Plans) | 1 | I.s. | \$45,000.00 | \$45,000 |
| TRAFFIC ITEMS |  |  |  |  |
| Trafficmen - Town (City) Police Officer | 480 | hr. | \$75.00 | \$36,000 |
| Trafficmen - Uniformed Flagger | 960 | hr. | \$55.00 | \$52,800 |
| Contract Items |  |  | SUBTOTAL | \$762,700 |
| Clearing and Grubbing Roadway |  | 2.0\% |  | \$15,300 |
| $M$ \& P of Traffic |  | 4.0\% |  | \$30,500 |
| Mobilization |  | 7.5\% |  | \$57,200 |
| Construction Staking |  | 1.0\% |  | \$7,600 |
| Minor Items |  | 25.0\% |  | \$190,700 |
| Inflation Factor | 0 | 5.0\% |  | \$0 |
|  |  | CONSTR | TION TOTALS | \$1,060,000 |
| CONTINGENCIES |  | 10.0\% |  | \$106,000 |
| INCIDENTALS |  | 25.0\% |  | \$265,000 |
| UTILITIES |  | 15.0\% |  | \$159,000 |
| TOTAL ESTIMATED COST |  |  |  | \$1,590,000 |

